

# A new high-precision and low-power GNSS receiver for long-term installations in remote areas

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**Abstract.** We have developed a new high-precision GNSS receiver specifically designed for long-term unattended deployments in remote areas. The receiver reports its status, and can be reprogrammed remotely, through an integrated satellite data link. It uses less power than commercially available alternatives while being equally, if not more, accurate. Data is saved locally on dual SD card slots for increased reliability. Deployments of a number of those receivers in several different locations on the Antarctic Ice Sheet have shown them to be robust and able to operate flawlessly at low temperatures down to -40 C.

## 1 Introduction

Long-term monitoring using permanently installed GNSS receivers is a powerful tool for geophysics research, and this technique is now commonly used in various different settings. Applications are too numerous to list but include measurements of glacier flow, tectonic movements, ground subsidence, and isostatic uplift, to name a few. In such applications the reliability of the system is of utmost concern as the GNSS units are often left unattended for prolonged periods of times.

Here we discuss the development and testing of a new simple-to-use, reliable, low-power and low-cost GNSS receiver unit, for use in remote areas. We describe the design and performance of a new GNSS unit that fits all those criteria. Although we believe our new GNSS receiver to be of general use for the wider geophysical sciences community, we will specifically focus on its application to remote polar areas. This is because our own primary application of GNSS receivers is to monitor the temporal variation in glacier flow in Antarctica.

Here we use the word “receiver” to include the signal tracking and control circuits, internal power supplies, communications and logging hardware. We do not include the antenna or field installation hardware.

### 1.1 The need for a new GNSS receiver

Field installations of GNSS receivers in remote areas require a reliable and sustainable power source. A common solution is the use of batteries with supplementary solar panels. In polar areas, where there is insufficient sunlight for much of the winter, wind turbines ~~or~~ are often employed as well together with large battery packs to ensure continuous power over period of low winds (Rose et al., 2009; Bauguitte et al., 2011). ~~Figures 1 and Figure 1 and Figure 2~~ shows a typical polar GNSS installation used by the British Antarctic Survey for over-winter deployment of GNSS units. As the figure shows the power-system is fairly large and the weight of these batteries, wind turbines, solar panels and their necessary scaffolding is not insignificant, and often determines the upper limit of the scope of any polar installation. The power consumption of a GNSS receiver therefore puts significant constraints on their applicability in remote areas.

Although commercial off-the-shelf (COTS) GNSS receivers can, and have been used, for long-term deployments in Antarctica (e.g. Dach et al., 2008; King et al., 2011; Anderson et al., 2013; Tregoning et al., 1999), and Greenland (e.g. Bevis et al., 2012; Nettles et al., 2008; Shepherd et al., 2009), they are not primarily designed for such applications. As a consequence, and as we will show below, the power consumption of such devices is higher than it needs to be. Furthermore, the numerous features of commercial GNSS receivers, many of which tend to be irrelevant for long-term static deployments, actually make such units less reliable and complicate their use.



**Fig. 1.** GNSS station installed on the Institute Ice Stream showing the two wind turbines and solar panels required to power the GNSS receiver.



**Fig. 2.** 6 100Ah batteries in 3 battery enclosures, for the field installation of figure 1. In total, the batteries and enclosures weighed 300kg, nearly half of the aircraft payload available for the site installation.

Based on our experience in the use of commercial GNSS monitoring systems in polar areas acquired over more than a decade, common sources of failure in long-term GNSS monitoring systems are due to corruption of the memory card, mechanical failure of the power supply, or user error whilst navigating their myriad configuration menus. The memory card failure rate is particularly problematic in polar installations: a survey of 30 memory cards retrieved from a variety of year long polar monitoring stations found that 4 had suffered a complete hardware failure whilst 3 were corrupted with partial loss of data.

Commercially available systems benefit from regular services, repairs and firmware updates. Although generally beneficial, for long-term deployments in remote areas such regular services and updates bring with them their own problems. Installing critical firmware updates on GNSS units that are only visited once a year may not always be possible. As an example, for a one brand of commercial GNSS units a num-

ber of observational GNSS campaigns by the British Antarctic Survey ([BAS](#)) have, in the recent past, been severely compromised as the GNSS units all stopped recording simultaneously due to a firmware error. Although the error was detected by the supplier well ahead of time, installing the firmware patch on all affected remote GNSS units was not possible.

To address the above listed problems we have developed a new GNSS receiver around the requirements of a long-term polar installation. The receiver uses less power than all commercial available alternatives known to us, while at the same time being more reliable, and at least equally, if not more, accurate. Henceforth this receiver design is referred to as **Ubi** the Latin word for “where”.

Module	Power	Accuracy	RTK
		DGNSS	Power supply
NovAtel ( <a href="#">Novatel, 2015</a> ) OEM628	1.3 W	0.4m	10mm
Trimble BD920 ( <a href="#">Trimble, 2014</a> )	1.3W	0.25m	8mm
Hemisphere Eclipse ( <a href="#">hemisphere, 2010</a> )	2.5W		10mm
<b>Ashtec Ashtech MB100 (<a href="#">Ashtech, 2014</a>)</b>	<b>0.95W</b>	<b>0.3m</b>	<b>10mm</b>
Septentrio AsteRx2el ( <a href="#">Septentrio, 2012</a> )	2.9W	0.5m	6mm

**Table 1.** Comparison of OEM precision GNSS receiver daughter board, values from manufacturer datasheets. The entry marked in bold is the board chosen for use in **Ubi**.

## 1.2 Design requirements

The four principle design requirements that we set out to meet with our new GNSS receiver, **Ubi** are that it should 1) be at least as accurate as equivalent COTS GNSS receivers, 2) reliable, 3) use as little power as possible, and 4) be simple to configure.

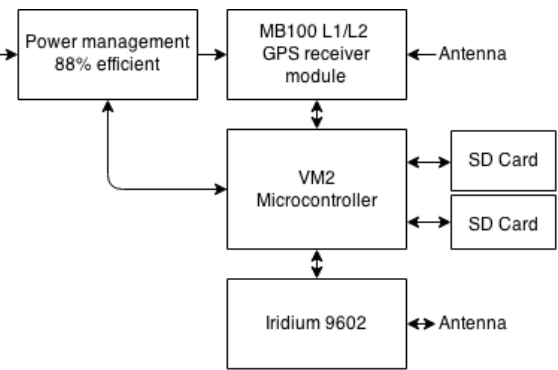
Discussions with operations managers and relevant scientists at UNAVCO, U.S., [the British Antarctic Survey \(BAS\)](#), [BAS](#) U.K., and at the Alfred-Wegener-Institute (AWI), Germany, furthermore highlighted the importance of the individual user being able to quickly assess the status of the unit. Therefore it was decided that the **Ubi** should have a status display indicating if the unit is logging, if the power supply is performing correctly, and whether the GNSS antenna is connected and working. For easier retrieval, and for planning repair and service visits, the **Ubi** should furthermore report its status and location periodically via a remote communications link. Finally, it should be possible to remotely reconfigure the **Ubi**. Thus, if the power supply is failing, or the battery supply is not sufficient for 24 hour operation over the winter period, the receiver can be re-configured to log for a fraction of the day instead, entering a low power sleep mode for the remaining period.

## 2 Ubi instrument design

The **Ubi** is mostly assembled from a number of off-the-shelf components. These include a GNSS receiver module, a micro-controller, and Iridium modem and antenna, a power management unit, and GNSS antenna. An overview of the principal components is given in figure 3 and figure 4 shows the internal hardware.

There are number of precision GNSS receiver units (i.e. dual frequency receivers) available, in the form of daughter boards, that can be integrated into a larger system. Table 1 compares the accuracy (in Differential GNSS (DGNSS) and on-board Real-Time Kinematic (RTK) position modes) and power consumption of five OEM receivers (values from their respective datasheets).

[Other GNSS receiver units exist that can record data from the GLONASS, Galileo and BeiDou satellite constellations](#)



**Fig. 3.** Diagram of receiver principle components.

[as well as GPS. These may be appropriate for future versions of Ubi as the coverage of these constellations increases, but for now we rejected these receivers due to their increased power consumption.](#)

After having evaluated available GNSS receiver boards, we decided to build the **Ubi** around the Ashtech MB100 L1/L2 GNSS receiver board. The MB100 was chosen over others for its low power consumption and [low-lower cost](#), while at the same time having similar accuracy as other boards (see Table 1).

The **Ubi** is build around a micro-controller (Micro-robotics VM2 ([MicroRobotics, 2015, D040](#))) which is responsible for configuring the GNSS receiver, managing its power supplies, monitoring its performance and logging the raw, unprocessed, GNSS data on to an SD card. The micro-controller is also responsible for organising the transmission of the **Ubi** status messages and processing reconfiguration commands via an Iridium 9602 modem ([Iridium, 2014, 27000 V3](#)).

As past experience has shown SD cards to be a significant source of unreliability, dual SD card slots are provided for increased reliability. At any given time data is written to only one of those cards. If data-write failure is detected, the system automatically switches to the other memory card.

### 2.1 Configuration options

The **Ubi** is configured by storing a simple, text-based configuration file on the SD card. Without such a file, the **Ubi** will use default configuration values. We have deliberately kept the programming of the units as simple as possible without limiting their intended use. As our system is intended for long-term recording of GNSS data and subsequent post-processing only, there is no need for any programming options related to any other uses. This greatly simplifies the use and the programming of the system. At present there are only three configuration variables that need to be set:

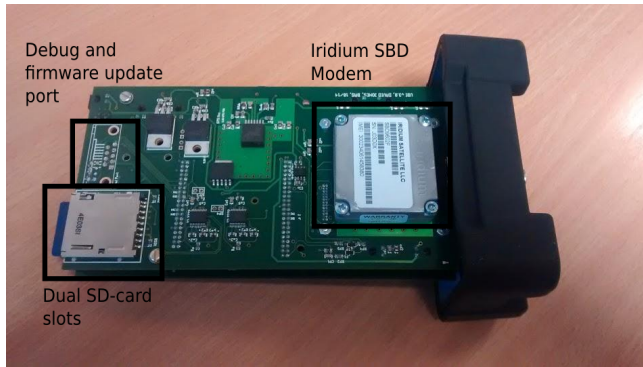


Fig. 4. Internal hardware of Ubi

1. The duration within each 24 hour period (synchronised at midnight) over which the **Ubi** records GNSS data (0-24 hrs, default 24). It will spend the rest of the time in a low-power idle mode.
2. The frequency of status update transmissions via the Iridium link, back to the user (1-365 days between messages, default 1 day).
3. The raw GNSS sample rate (1-300s).

The raw GNSS data ~~is~~ ~~are~~ stored in a compressed ATOM format (Artushkin et al., 2008) which is simple to convert to standard RINEX formatted files.

## 2.2 Remote interface

An Iridium modem provides a two-way datalink between the **Ubi** and the user at a remote location. This is a low bandwidth link that is not intended for transferring the large GNSS datasets but for supervision and reconfiguration purposes only. Regular updates from the **Ubi** describe its configuration, location, power supply voltage and available file-space, details which are displayed or plotted through a website (see figure 5). The user can reconfigure the logging period, status update frequency and GNSS sample rate of the **Ubi** via this same website.

The Iridium communications system was chosen over alternatives because it can be used in the Antarctic with a small antenna, is a low cost and low power consuming (45mA average) modem.

The advantage of this remote reconfiguration capability is the flexibility to respond to changing environmental conditions. For instance, if installing large battery packs and wind turbines is impractical, the **Ubi** can be configured to record for 24 hours a day when there is sufficient solar power, or for shorter periods when there is not.

The transmitted updates from the **Ubi** will also give an insight into any failures. For instance, if the power supply is failing this will be evident in the reported battery voltage.

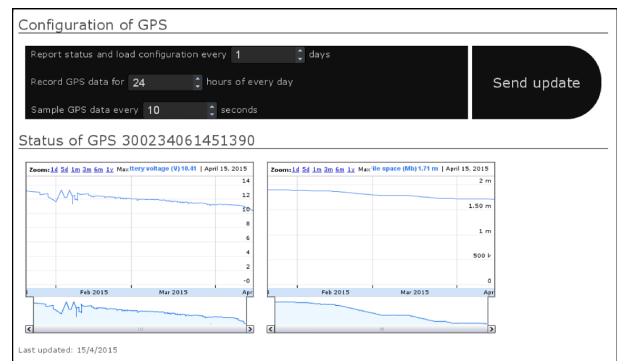


Fig. 5. Web interface for remote re-configuration of the **Ubi** receiver.

If the GNSS antenna or ~~Ashtec~~ ~~Ashtech~~ modem have failed this will be evident in the use of file-space. Finally if the **Ubi** stops transmitting updates the end-user can conclude there has been a complete system failure. Based on this information the end-user is better equipped to plan for the next site visit.

## 2.3 External hardware

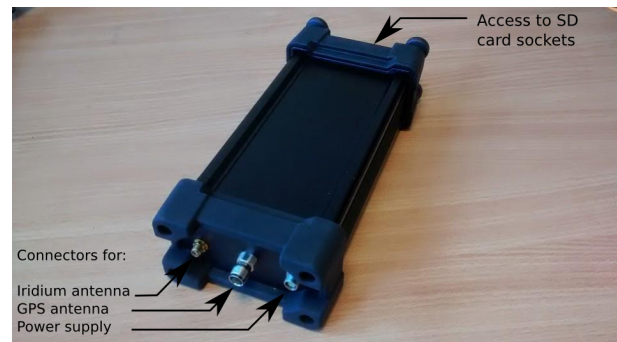


Fig. 6. Ubi case design



GNSS receiver	Power consumption	Predicted lifetime
Leica GS10	3.25 W	18.5 days
Trimble R7	2.5W	25 days
<b>Ubi</b>	<b>2.0W</b>	<b>29.5 days</b>

**Table 2.** Comparison of GNSS receiver power consumption.

Ubi is consists of 2 PCBs that have a conformal coating to protect them from moisture. These are housed in a weather-proof IP67 case (see figure 6). Three ports protrude from one end, an SMA connection for the Iridium antenna port, a TNC connection for the GNSS antenna port and a four pin Lemo connector for power and serial communication.

The other end of the case features 4 leds visible behind an enclosed window. These enable the end user to quickly validate the correct operation of the power supply, the file system, the GNSS antenna and the Iridium antenna, as well as the **Ubi** itself. This end is fastened in place with four thumb screws so as to make accessing the SD cards simple.

### 3 Test results

#### 3.1 Power consumption

Table 2 compares the power consumption of the **Ubi** with two commonly used COTS GNSS receivers. The power consumption values listed are measured and include the power needed to supply an active GNSS antenna (**Leica AS10**). The lifetime figures are an estimate of how long the receiver will operate on 2 100Ah batteries at -30C.

From table 2 it can be seen that the **Ubi** receiver uses less power than currently available COTS receivers when recording GPS data. Thus the **Ubi** will run for longer when deployed with a battery power supply.

Of the 2.0W power consumed by the Ubi 0.95W is for the GPS receiver, 0.35W is for the GPS antenna and 0.7W is lost due to power supply voltage conversion. When the status LEDs are active (during the first hour of operation), a further 0.03W is used, and whenever the iridium transmits data it uses a further 0.95W.

#### 3.2 Kinematic tracking accuracy

The comprehensive assessment of the accuracy and precision of a GPS receiver is difficult, expensive (Jackson et al., 2000; UNAVCO, 2012; Penna et al., 2012) and subjective — different conclusions can be drawn depending on the form of the experiment and the type of post-processing performed. These assessments normally consist of several different measurement types, performed on data from one or more of the receivers under evaluation. Here we use three separate types of metrics to evaluate the accuracy of GPS positions calculated from data recorded by Ubi . By themselves, none of these metrics are a conclusive measure

of the absolute performance of Ubi but, taken as a whole, their results can be considered indicative of the relative performance of Ubi

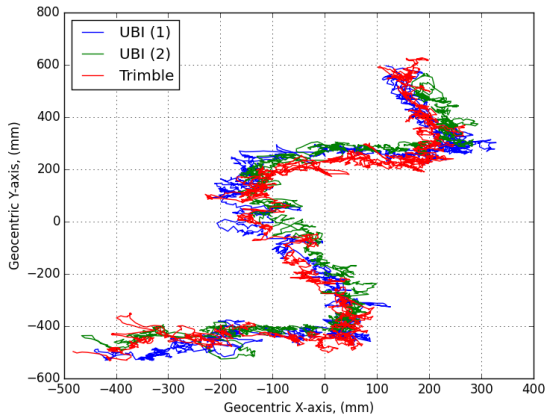
A network of **Ubi** receivers has been installed next to a Trimble R7 receiver from a different project (Anderson et al., 2013) on the Brunt Ice Shelf, Antarctica. This ice shelf has a typical daily vertical tidal movement of 1m, and the GNSS data ~~was~~ were processed with the kinematic precise point positioning (kPPP) technique. We use the GIPSY/OASIS (Zumberge et al., 1997) GNSS data processing package to perform the kPPP analysis. Figure 7 shows the recorded horizontal movements of three of these receivers, each 20 metres apart, from 24 hours of data. Two of these receivers were **Ubi** units (**Ubi(1)** and **Ubi(2)**) and one was a Trimble R7 receiver. All were equipped with the same type of GNSS antenna (Leica AS10).

The receivers were all attached to a fixed infrastructure, so their relative position did not change. For ease of comparison between these three receivers, the mean position of each receiver has been subtracted from the displacement curves shown in Fig. 7. As the figure shows, these three displacement curves overlap almost perfectly. Hence, the horizontal displacements as determined by these three receivers are almost identical, and their accuracy therefore comparable.

A further insight into the performance and the accuracy of the receivers is gained by calculating the temporal variation in the distances between the receivers, see figures 8 and 9. As mentioned above all three receivers were attached to the same platform and the distance between them did therefore not change with time. Calculating the pair-wise distance at each 30s interval between all the three receivers gives three time series of baseline lengths. We analysed the scatter in those three time series, i.e. the fluctuations in calculated baseline lengths around their respective mean values. Doing so revealed that that the scatter was smallest for the **Ubi(1)** to **Ubi(2)** baseline, and somewhat larger for the two **Ubi(1)** to Trimble R7 and the **Ubi(2)** to Trimble R7, baselines (see Fig. 9). Possibly the smaller scatter in the **Ubi(1)** to **Ubi(2)** baseline is simply related to the two **Ubi** receivers having similar error characteristics resulting in cancellation of errors as the baseline length is calculated, but nevertheless this experiment shows that the **Ubi** is at least comparable in accuracy to the Trimble R7 GNSS receiver.

#### 3.3 Static position analysis accuracy

This trial was conducted at the British Antarctic Survey headquarters in Cambridge. An **Ubi** receiver and a Trimble R7 receiver are installed on the roof with a largely unobstructed view of the sky. Both receivers shared a common choke-ring antenna (Novatel ANT-533) via a two-way powered splitter. The GIPSY/OASIS software was used to generate position estimates and ~~double difference~~ phase residuals. Seven 24-hour, 10 second interval files were collected from each receiver. The only change to the default configuration of each



**Fig. 7.** Kinetic-Kinematic tracking of the Brunt ice shelf over the period of 24 hours

receiver was to set the minimum satellite track elevation to be zero degrees.

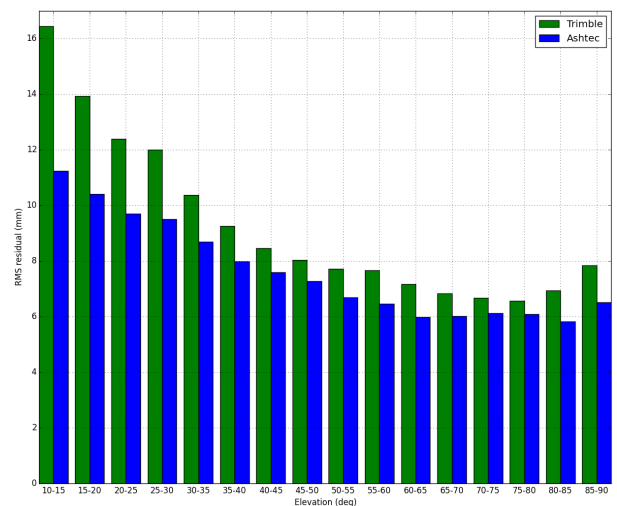
Due to the unobstructed view of the sky available to the antenna and the long duration of this experiment, we are confident assuming that there is no bias in the calculated positions; that we can use the mean calculated position as a reference point.

The carrier-phase residuals from each satellite are a measure of the uncertainty of a position calculation noise in the recorded observations. Figure 10 shows the root-mean-square average of the phase residuals, binned by the calculated angle of elevation of each satellite relative to the receiver in 5-degree intervals. The y-axis is the residual in millimetres. Each bin is a seven-day average of the computed L2 band residual. At all elevations the residuals of the Trimble were the highest. This is an indication that the **Ubi** is the more precise accurate receiver.

Figure 11 shows the scattering of the positions calculated by GYPSY/OASIS over the same seven-day period. The data is split into both 7 x 24 hour segments, and 84 x 2 hour segments prior to processing. The scattering of the positions calculated from 24 hour data segments is similar for both receivers, however the outliers from the positions calculated from 2 hour segments are all from the Trimble receiver.

### 3.4 Reliability

As mentioned above, the mal-functioning-malfunction of memory cards is a common reason for data loss. For that reason, our system uses two memory cards and switches from one to the other if a data-write failure is detected. **Ubi** was tested with for various combinations of a functioning SD and non-functioning SD cards. (These test were conducted in conjunction with Dr. Dominic Wilson, at Cambridge Data Recovery.) In total ten non-functioning SD cards were used, three suffering from software malfunctions, and the remain-



**Fig. 10.** Residual analysis measure of accuracy of **Ubi** and Trimble receivers in Static mode

ing seven from hardware malfunctions. Of the three cards with software malfunctions, **Ubi** correctly detected the fault and switched to use the alternate SD card. Of the seven cards with hardware malfunctions, **Ubi** operated correctly for five of them. The two cards for which it failed were both a low-cost generic brand that failed by saturating the communications bus with the micro-controller. This could be overcome in future versions of **Ubi** by using a buffered communications bus.

Ultimately, the reliability of the **Ubi** receivers is best tested through long-term field deployment under realistic conditions. Twelve of these **Ubi** receivers are currently installed in component modules of the Halley VI Antarctic research station. This network of receivers is providing a high quality record of the movement of modules and the overall distortion

[deformation](#) of the Halley VI station (Jones and Rose, 2015). The receivers are installed within the station so are not exposed to harsh polar conditions. These receivers have cumu-  
 360 latively recorded two years worth of data without failing. 410

Furthermore, two prototype receivers were installed in February 2014 outside the Rothera Antarctic research station. These receivers successfully recorded three months of  
 365 data each before their common power supply failed. Upon 415 retrieval the receivers were found to be intact and fully operational.

Another set of two receivers were installed in February of 2015 as part of long-term trials, one at Rothera whilst the  
 370 other is being tested by UNAVCO at the McMurdo Antarctic 420 research station. So far both have operated flawlessly for three months and have not shown any signs of failure.

### 3.5 Benefits of the Ubi receivers

The lower power consumption of the **Ubi** receivers as compared to other typically deployed commercial systems allows  
 375 for substantially smaller power-supply systems to be used. When deploying system using [aircraftsaircraft](#), where total  
 380 weight of the system is often the limiting factor affecting the 430 design of a GNSS network, the resulting weight reduction can have important consequences.

As an example, in January 2013 we set out to install three commercial GNSS receivers on Institute glacier  
 (81°S, 76°W), Antarctica, in a single [flight from a Twin Otter aircraft flight](#). Two power systems were designed for this  
 385 installation, a summer only system weighing 140 kg, and a full 435 year system weighing 410 kg. Under BAS safety criteria our aircraft can take off from and land on snow runways with a maximum payload of 2200 kg. Of this payload 250 kg were passengers, and as the nearest fuel depot was 245 km away we needed 1250 kg of fuel, allowing for a potential 700 kg  
 390 of cargo. Thus we were able to install no more than one full 440 year system and two summer only systems. Had we instead of using commercial GNSS systems, used the **Ubi** receiver, we could have installed a greater number of such units under  
 395 the same logistical constraints. Furthermore, the remote programming capability of the **Ubi** system would have allowed us to make better use of the available power. For example, using the same summer-only power system, **Ubi** could have  
 400 been programmed to log an estimated eight hours of each day 445 during the winter (derived from table 2), and then to switch to a 24 hr logging mode during the summer. If this setup had been available in 2013 we would have had the payload capacity necessary to install four **Ubi** receivers instead of three,  
 405 still allowing for the extra fuel needed for a fourth site visit. 450

## 4 Conclusions

We have developed, tried and tested a new GNSS receiver specifically designed for long-term deployments in polar ar-  
 455

reas under harsh conditions. Our GNSS receiver, **Ubi** uses less power than existing commercial GNSS receivers, reducing the necessary batteries, solar panels and wind turbines needed for long-term GNSS monitoring. [The external interfaces of Ubi are common to those of existing GNSS receivers, so installation of Ubi does not require significant changes to existing setup procedures.](#)

The system allows for a two-way communication via an Iridium link. The status of the **Ubi** receiver is broadcast, and the unit can be reprogrammed remotely. The ability to remotely reconfigure the **Ubi** logging period in response to the availability of solar power creates further opportunities to reduce the size and weight of these power system components.

[The individual components of a single Ubi receiver can be procured for less than £2000, making this potentially significantly cheaper than commercial alternatives.](#)

The **Ubi** receiver is at least as accurate as [some](#) commercial GNSS receivers commonly used for long-term monitoring. It is easy to configure and has improved status reporting features. We have made the **Ubi software-firmware** open-source [\(under the GNU version 2 license\)](#) and available at <https://github.com/antarctica/UBI>. This will allow other polar scientists to evaluate, use, adapt and improve upon the design for the benefit of all in the community. [It is simple to load the Ubi with new firmware via a serial port interface.](#)

[The Ubi receiver has one external serial port interface, and has connections for another. It also has connections for general purpose digital and analogue, inputs and outputs. As such it can be easily adapted to log external data feeds or control power lines based on commands triggered by a timer or the Iridium lin.](#)

## 5 Acknowledgements

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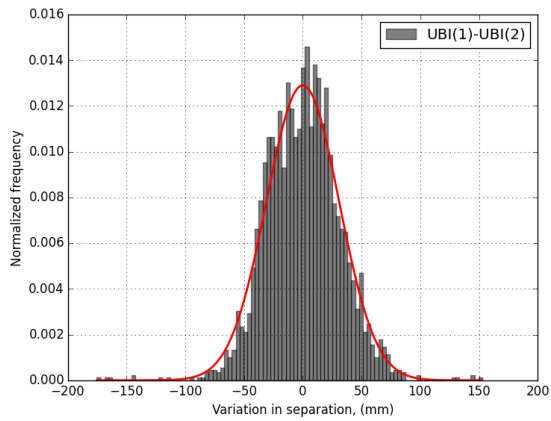
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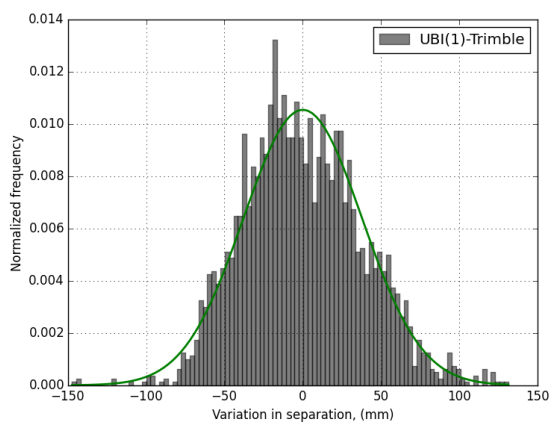
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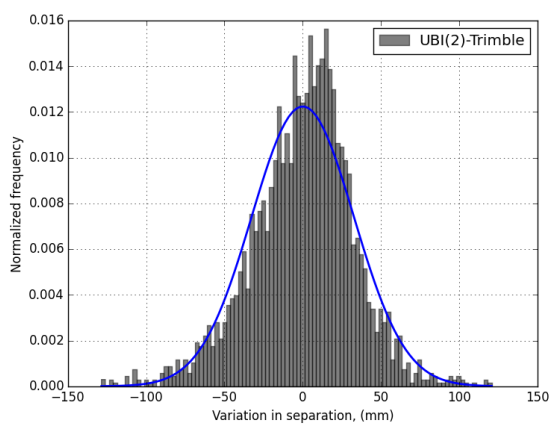




(a)

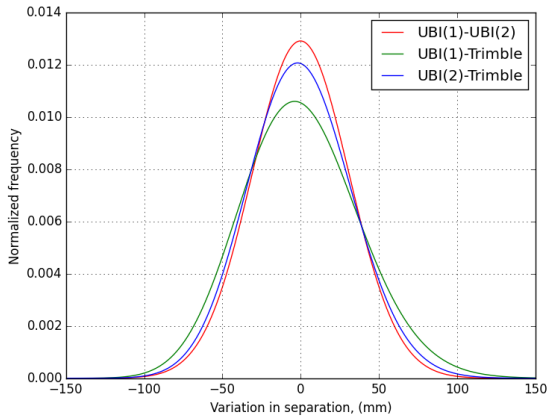


(b)

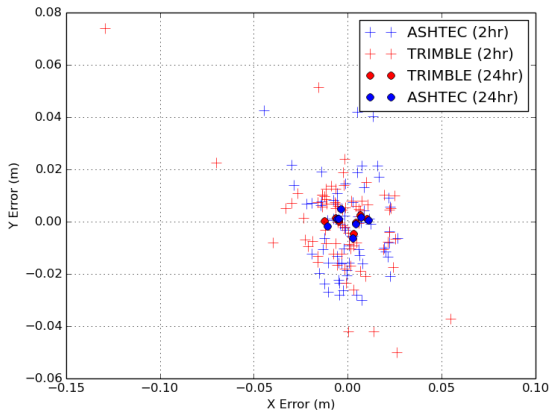


(c)

**Fig. 8.** Histogram of variation in separation between receivers (a) Ubi(1) and Ubi(2), (b) Ubi(1) and the Trimble R7, (c) Ubi(2) and the Trimble R7



**Fig. 9.** Gaussian fit to temporal variations in pair-wise distances between two **Ubi** receivers and a third Trimble R7 receiver. The GNSS data from each receiver was processed independently of the data from the other receivers using a kinematic precise point processing technique (kPPP). All receivers were attached to the same platform (with approximately 20 m separations), and the widths of the Gaussian curves therefore directly reflect baseline errors. As can be seen, the baseline errors are on the order of about 5 cm, an accuracy expected for short term kPPP occupation and similar for each receiver pair.



**Fig. 11.** Comparison of accuracy of **Ubi** and Trimble receivers in Static mode