

Dear Lev Eppelbaum (levap@post.tau.ac.il)

We appreciate your help in editing the work. We would like to present the response to reviewers' questions and comments as well as marked-up changes (red color into the text) because of the review process which we had to make to improve the paper.

The changes which were made in view of Anonymous Referee #1 report – First Reviewer:

Records in the old version of manuscript (GI Discussion)	Reviewer's questions (Q) and comments (C)
Records with changes in the revised manuscript	Authors' responses (R)
21-22	<b>Q1.</b> Page 1, Line 21 – "Single point positioning (SPP) allows of the indication of an autonomous position of a receiver using code data from the Global Positioning System (GPS)." Does the SPP positioning technique concerns only the GPS system or also other GNSS systems?
21 - 22	<b>R1.</b> The SPP positioning technique concerns the GPS and other GNSS systems, e.g., GLONASS, GALILEO, or BeiDou. The idea was to use the real code data in the numerical experiment from the GPS because of the system's popularity, availability, and declared precision comparing to other mentioned GNSS systems.
149-159	<b>C2.</b> Equation (9). Not all values in the formula have been explained in the text of the article.
150 - 161	<b>R2.</b> All symbols are explained in the new version of manuscript.
183	<b>Q3.</b> Equation (14). If V, X and L are vectors so why then they are written in capital letters?
183 (183 – 203)	<b>R3.</b> This is our mistake. The symbols of vectors were corrected as the reviewer's suggestion.
187	<b>C4.</b> Equation (16). The paper only presents the method of calculating the "mapcoeff" coefficients. Please provide information about determination of the rest of coefficients of matrix.
187 - 191	<b>R4.</b> Information about determination of the rest of coefficients of matrix is included in the corrected version of manuscript.
198-201	<b>C5.</b> Equations (20, 21). Least squares solution is widely known in geosciences and I think it can be omitted from the article.
In the improved paper equations do not exist.	<b>R5.</b> The formulas of LS solution have been removed in the new, improved version of manuscript.
211	<b>C6.</b> Equation (22) . It must be underlined that this formula of the Euclidean distance between points in 3D space is the basic knowledge, so in my opinion there is no need to write this quantity as a new formula.
209 - 217	<b>R6.</b> The terms from formula (22) are applied in formula (24). Therefore we decided to present them explicitly, in spite of the basic knowledge of the Euclidean distance formula. <u>Note, the number of mentioned equations (22) and (24) are in the revised version of manuscript as follows: (20) and (22).</u>
216	<b>C7.</b> Equation (24). The quantities in the denominator are not explained in the text.
214 - 217	<b>R7.</b> The terms of equation (24) were briefly explained in the revised version of the research paper. <u>Note, the number of cited equation in the revised form of paper is (22).</u>
-	<b>Q8.</b> Can the approach described in the paper be generalized by combining of the observations from different GNSS systems? If yes, then how would the computational procedure looks then?
-	<b>R8.</b> Yes, the approach described in the paper can be generalized by combining of the observations from different GNSS systems. First of all, the appropriate observational data from other GNSS systems have to be derived. Taking into account equations (8) and (10), the various variants of them should be considered because of different carrier frequencies of satellite signals from utilized GNSS systems as well as

	<p>equation (13), related to <i>mapcoeff</i> calculation component. The equation (4) will remain unchanged. The mapping function as well, due to subsequent satellites zenith angles of different GNSS systems at the piercing point. Note, that the value of <math>VTEC_0</math> would be still equal to 5 TECU. Undoubtedly, this quantity can be changed during another experiment containing more than one GNSS system. Taking into account equations (9) and (11), the existed set of GPS code equations should be supplemented by the new observation formulas using satellites of subsequent GNSS systems. The appropriate ingredients of mentioned formulations should be generated in relation to available satellites of GNSS systems, e.g. tropospheric or ionospheric correction components. Afterward, the matrix notation (14) will be updated by magnification of matrices and vectors structure due to additional observations from following GNSS systems.</p> <p>Nevertheless, the combination of observations from different GNSS systems can be considered as an interested idea of the next numerical experiment to verify the reliability of SPP with autonomous method of ionospheric delay estimation.</p>
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The changes which were made in view of Anonymous Referee #2 report – Second Reviewer:

Records in old version of manuscript (GI Discussion)	Reviewer's questions (Q) and comments (C)
Records with changes in the revised manuscript	Authors' responses (R)
145	<b>Q1.</b> Equation (7): based on cited literature: Leick et al., 2015, the argument of the trigonometric function is a zenith angle at the piercing point. Is it the case in the proposed algorithm?
146	<b>R1.</b> This is our mistake. The cited algorithm is referred to the zenith angle calculation at the observing site (from observer's view). The corrected formula was made in the updated version of manuscript. That was a separate mistake in the quoted algorithm because the formula used in the code in the MATLAB environment during numerical experiment was implemented correctly.
187	<b>C2.</b> Equation (16): The authors should give the formulas for calculating the entries of the design matrix A.
187 - 191	<b>R2.</b> The formulas for calculating the individual components of the design matrix A were implemented in the revised form of manuscript.
183 - 204	<b>C3.</b> Equation (14), (15), (17), (18), (20): I suggest to denote vectors with small, bold letters.
183 (183 – 203)	<b>R3.</b> The suggested matrix designations were done in the improved version of scientific research.
197	<b>C4.</b> Equation (19): In my opinion, the weight matrix should be denoted as W instead of P.
200	<b>R4.</b> The recommended symbol for the weight matrix was changed as the reviewer's suggestion. (In addition, the names of matrices were changed in view of better understanding: V => e – theoretical correction, A – matrix of coefficients without changes, x – vector of unknown parameters, C <sub>x</sub> – covariance matrix without change, m <sup>2</sup> <sub>0</sub> – variance factor without change as well).
216	<b>C5.</b> Equation (24): Consequently, the name of the gradient vector should be changed. The calculation of the entries of the gradient vector should be explained.
215	<b>R5.</b> The consequence of the weight matrix designation change is the need for the gradient name change as well. Therefore, the remark was positively included in the corrected version of the manuscript. <u>Note, in the revised version, the number of cited equation is (22).</u>
369 - 379	<b>C6.</b> The authors should describe the results listed in Table 3 in more detail.
372 - 381	<b>R6.</b> Basically, the results contained in Table 3 are quite close. Hence, we decided to make the extended description according to the reviewer's suggestion, including the similarity of the values of mean errors of coordinates differences in the NEU system on the comparable level.

# 1 **Single Point Positioning with Vertical Total Electron Content** 2 **estimation based on single epoch data**

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6 **Abstract.** This paper proposes a new mathematical method of ionospheric delay estimation in single point positioning (SPP)  
7 using a single-frequency receiver. The proposed approach focuses on the  $\Delta VTEC$  component estimation (MSPPwithdVTEC)  
8 with the assumption of an initial and constant value equal to 5 in any observed epoch. The principal purpose of the study is  
9 to examine the reliability of this approach to become independent from the external data in the ionospheric correction  
10 calculation process. To verify the MSPPwithdVTEC, the SPP with the Klobuchar algorithm was employed as a reference  
11 model, utilizing the coefficients from the navigation message. Moreover, to specify the level of precision of the  
12 MSPPwithdVTEC, the SPP with the IGS TEC map was adopted for comparison as the high-quality product in the  
13 ionospheric delay determination. To perform the computational tests, real code data was involved from three different  
14 localizations in Scandinavia using two parallel days. The criterion were the ionospheric changes depending on geodetic  
15 latitude. Referring to the Klobuchar model, the MSPPwithdVTEC obtained a significant improvement of 15 – 25% in the  
16 final SPP solutions. For the SPP approach employing the IGS TEC map and for the MSPPwithdVTEC, the difference in  
17 error reduction was not significant, and it did not exceed 1.0% for the IGS TEC map. Therefore, the MSPPwithdVTEC can  
18 be assessed as an accurate SPP method based on error reduction value, close to the SPP approach with the IGS TEC map.  
19 The main advantage of the proposed approach is that it does not need external data.

## 20 **1 Introduction**

21 **Single point positioning (SPP) allows of the indication of an autonomous position of a receiver using code data from**  
22 **different Global Navigation Satellite Systems (GNSS).** Code ranges are not ambiguous and do not require to apply the  
23 precise method of ambiguity initialization (Bakula, 2020). The principal problem of SPP stems from different types of errors  
24 degrading the GPS signal between a rover and a specified satellite in a given epoch. Ionospheric delay contributes to the  
25 general GPS error budget by its volatility in the range of 40 – 60 m during daytime and 6 – 12 m at night (US Army Corps of  
26 Engineers, 2003).

27 The ionosphere consists of charged particles that appear because of the ionization process (El-Rabbany, 2002; Awange,  
28 2012). Problems with ionosphere modeling come from difficulties between solar activity and the geomagnetic field  
29 interactions (Xu and Xu, 2016). The basic concepts of the GPS signals delay were briefly considered by Golubkov et al. and

30 Kuverova et al. (Golubkov et al., 2018; Kuverova et al., 2018; Golubkov et al., 2019). To specify a suitable magnitude of  
31 delayed GPS signal along an appropriate path between satellite and receiver, a proportional quantity such as Total Electron  
32 Content (TEC) has to be involved and defined as the linear integral of the density of the particles alongside the ray path  
33 (Cooper et al., 2019). The TEC unit is equal to  $10^{16}$  electrons per square meter (in the cross-section of  $1 \text{ m}^2$ ) (Ciraolo, 2005).  
34 To calculate and reduce such effect on the GPS code measurement, Stępiak (2016) distinguished different types of models  
35 and mathematical estimating methods: physical - theoretical (e.g. Chapman's model), physical - empirical (e.g. IRI and the  
36 NeQuick model), mathematical - deterministic (based on a mathematics function), and mathematical – stochastic (based on a  
37 large set of processed data used to describe the spatial-temporal changes of ionosphere) e.g. the IGS model.

38 The authors propose the autonomous SPP approach with  $\Delta VTEC$  component estimation using single-frequency GPS  
39 code observations to be independent of external products, e.g. an IGS TEC map. The disadvantage of the mathematical  
40 models is performing an ionospheric effect calculation mostly in post-processing. Since many mathematical approaches to  
41 self-sufficient ionospheric delay modeling have been proposed, especially in the carrier phase domain using multi-frequency  
42 observations, the authors wanted to introduce a new estimation method employing single-frequency GPS code observations.  
43 For instance, Georgiadiou (1994) proposed a mathematical method based on differences between the pseudo-ranges  
44 measured on the L1 and L2 carrier frequency, respectively (dual-frequency method). The computational tests with  
45 comparison to the reference method without ionospheric corrections were done by Camargo et al. (2000), focusing  
46 particularly on the pseudo-ranges filtered by the carrier phase. The method of slant delay estimation (STEC – alongside a  
47 line of sight) in the L1 carrier reduced 80% of errors related to ionospheric effects in the point positioning technique, also  
48 delivering improvement solutions during the ionosphere maximum. Bosy (2005) described a geometry-free linear  
49 combination which can be employed to ionosphere modeling, with simultaneous consideration and repair of cycle-slip  
50 effects and other parameters of GPS vector - ambiguity and tropospheric effects. Krypiak-Gregorczyk and Wielgosz (2018)  
51 proposed the use of multi-frequency GNSS signals for TEC modeling, utilizing the carrier phase bias of a geometry-free  
52 linear combination. The received bias accuracy results on the level of 7 – 8 cm allow TEC computation with desirable  
53 uncertainty, i.e. lower than 1 TECU. Additionally, an ionosphere-free linear combination as an independent positioning  
54 approach can also be well adapted to minimize the ionosphere negative impact on GPS positioning (Teunissen and  
55 Kleusberg, 1998). However, Hofmann-Wellenhof et al. (2008) stated that “ionosphere-free” is not an entirely correct name,  
56 caused by the approximation existing in the process of making the refractive index. Those authors studied an ionosphere-free  
57 approach in the code SPP and achieved a beneficial magnitude of error reduction (50-60%) in relation to the reference SPP  
58 model without ionospheric corrections.

59 On the contrary, empirical models do not significantly reduce the ionosphere influence in the GPS positioning as  
60 mathematical (deterministic) methods, but can make real-time improvements by using the external data, e.g. coefficients  
61 transmitted in the navigation message to correct the signal pseudo-ranges. One of these is the Klobuchar algorithm (see  
62 Klobuchar, 1987), which compensates for 50 – 60% of the ionospheric range error, utilizing a single-layer model of the  
63 ionosphere (Leick et al., 2015). In the current study, the authors wanted to treat the SPP method with the Klobuchar

64 algorithm as a reference method, because of its popularity and utility in GPS measurement. A significant improvement can  
65 be noted in the vertical component which is the most affected by the atmospheric delay. Júnior et al. (2019) investigated the  
66 analysis of the Klobuchar model in the ionospheric delay reduction procedure utilizing code observation in point positioning.  
67 The algorithm works clearly when ionosphere activity is significant and improves vertical solutions by 67%. For the  
68 horizontal components, the improvement using the Klobuchar algorithm is up to 9% regarding the non-iono model. It should  
69 be noted that GPS point positioning using the Klobuchar algorithm can degrade the position because of the constant value of  
70 the ionospheric delay (up to 5 ns SET) during nighttime.

71 High-quality representation of the ionosphere influence on positioning can be obtained by the Global Ionospheric  
72 Models (GIMs), used mostly in the post-processing purposes as explained in Ciećko and Grunwald (2020). It is worth noting  
73 that Abdelazeem et al. (2016) developed the regional ionospheric model over the European area and implemented it in  
74 Precise Point Positioning (PPP), operating in real-time using the real-time service products (RTS) of the International GNSS  
75 Service (IGS). The results present an improvement in the accuracy on the level of 40 % (under the mid-latitude region) in the  
76 3D position relating to the IGS-GIM. The accuracy is higher primarily because of the better temporal and spatial resolution  
77 of the model ( $15'$  and  $1^\circ \times 1^\circ$ ), while the IGS TEC map includes nodes containing the appropriate VTEC value with a time  
78 resolution of 1 hour and a spatial resolution of  $2.5^\circ \times 5^\circ$ , respectively for latitude and longitude. In turn, Krypiak-Gregorczyk  
79 et al. (2017) prepared the ionosphere model covering the Europe region as well, based on multi-GNSS data. The solutions  
80 are beneficial because they have 2-3 times lower RMS value than the results of GIMs, e.g. from IGS. Zhang et al. (2019)  
81 also examined global ionospheric maps operating in real-time, dedicated to single-frequency positioning. Chen and Gao  
82 (2005) tested the IGS TEC map as the basic condition to assess the precision of the PPP model using different procedures to  
83 resolve the ionospheric delay problem such as single-frequency ionosphere-free linear combination (averages un-differenced  
84 code and carrier-phase observations on the same frequency) or estimation of the ionospheric effect as an unknown  
85 parameter. The advantage of the methods is no need for external products. For instance, the estimation method achieved  
86 comparable accuracy in the mid-latitude stations but for the higher latitude, the GIM is still quite better, inversely on the  
87 equatorial stations. This encourages a focus on the IGS TEC map as the high accuracy product to authenticate solutions from  
88 the suggested approach to SPP, and to validate the autonomous method of the ionospheric delay calculation. It should be  
89 noted that although the efficiency of GIMs is not significant using GPS code observations, the accuracy is suitable enough  
90 for navigation goals and further development of this concept.

91 In sum, the motivation of this paper is to analyze a new mathematical method of ionospheric delay estimation to  
92 improve the SPP. The authors put forward the hypothesis to be independent of external data use in the meaning of the new  
93 method in the ionospheric delay calculation procedure.

## 94 **2 SPP mathematical models**

95 In this section, the grounds of the common used SPP mathematical models using Klobuchar algorithm and IGS TEC  
96 map will be introduced, and the proposition of the new strategy of SPP determination by use of simple as well as

97 autonomous method to estimate the ionospheric delay. This is followed by the appropriate algorithm presentations with  
 98 suitable explanations. In addition, the accuracy analysis criteria will be described in view of models credibility procedure.

## 99 **2.1 SPP with ionospheric corrections using Klobuchar algorithm and IGS TEC map**

100 In this study, the Klobuchar model was adapted as a reference in the SPP accuracy tests. Eight model coefficients  
 101 transmitted via navigation message are the primary components involved in the algorithm to reduce the ionosphere effect in  
 102 the SPP. The geodetic coordinates of the GPS antenna, GPS observing time (in seconds) as well as azimuth and elevation of  
 103 observed satellites as viewed from the receiver are needed to be known. The formula to calculate the ionospheric correction  
 104 based on the Klobuchar algorithm is as follows (Hofmann-Wellenhof et al., 2008):

$$105 \quad \Delta T_V^{Iono} = A_1 + A_2 \cos\left(\frac{2\pi(t-A_3)}{A_4}\right) \quad (1)$$

106 where  $A_1$  is a constant value of 5 ns. In turn,  $A_2$  is a sum of multiplying four  $\alpha$  coefficients and the geomagnetic latitude of  
 107 an ionospheric pierce point  $\phi_{ip}^m$ .  $t$  means GPS time of the ionospheric pierce point.  $A_3$  is 14:00 local time which specifies the  
 108 highest ionospheric disturbance.  $A_4$  means the same as  $A_3$  but there are four  $\beta$  coefficients are multiplied by  $\phi_{ip}^m$ .

109 To obtain an ionospheric delay alongside the GPS signal travel path, the mapping function should be employed. Thus,  
 110 the concept of the ionospheric point has to be expanded as a piercing point of the GPS wave path and the  
 111 ionospheric single layer on the specified altitude. Thus, the satellite zenith angle at the piercing point -  $z'$  should first be  
 112 indicated (Hofmann-Wellenhof et al., 2008):

$$113 \quad \sin z' = \frac{R_e}{R_e + h_m} \sin z_0 \quad (2)$$

114  $R_e$  is Earth radius 6370 km and  $z_0$  means a zenith angle from the observing site.  $h_m$  is defined as the height of the ionospheric  
 115 pierce point. In general,  $h_m$  is identified by the single-layer model where all free electrons are concentrated in the infinitesimal  
 116 spherical shell at the assumed altitude - 450 km. Other formulations are possible too, for instance, from the Klobuchar  
 117 algorithm, presented in Rui et al. (2011):

$$118 \quad mF = 1 + 16 \cdot \left(0.53 - \frac{E}{\pi}\right)^3 \quad (3)$$

119 where  $E$  means an elevation angle in the slant factor calculation.

120 It should be also noted that the type of mapping function in the atmospheric effect calculation process contributes to the  
 121 final solution accuracy as well. Allain et al. (2009) examined the tomographic mapping function known as Multi-Instrument  
 122 Data Analysis System (MIDAS) to ionospheric effect determination for the single-frequency data. Research has shown that  
 123 daily positioning errors are up to 50% lower in comparison to positioning using the Klobuchar algorithm or International

124 Reference Ionosphere (IRI) when the surrounding distribution of receivers is favorable. Regardless of the map type, dual-  
 125 frequency observations allow for even greater precision of the ionospheric effect mitigation in the GPS pseudo-range  
 126 measurement.

127 Therefore, the mapping function can be used as an inverse of the cosine function (Hofmann-Wellenhof et al., 2008):

$$128 \quad \Delta T_s^{Iono} = \Delta T_v^{Iono} / \cos z' \quad (4)$$

129 Finally, the ionospheric delay alongside the rover-satellite is achieved in seconds. To obtain the metric magnitude of  
 130 the calculated effect,  $\Delta T_s^{Iono}$  is multiplied by the speed of light. The Klobuchar algorithm was fully described by Xu (2007).

131 To future elaboration,  $\Delta T_s^{Iono}$  will be denoted as  $\delta_K$  where subscript is appropriate for the Klobuchar method.

132 The second approach is SPP with ionospheric corrections computed based on the IGS TEC map. This method is used to  
 133 examine and verify the quality of the new autonomous, estimation method of the ionospheric effect in the SPP.  
 134 Consequently, ionospheric delay as the base formula in the zenith direction can be introduced (Schüler, 2001):

$$135 \quad \delta_{I_r} = \int_{h_m}^{\infty} \frac{C_2}{f^2} = \frac{C}{f^2} \int_{h_m}^{\infty} N_e(h) \cdot dh = \frac{C}{f^2} \cdot VTEC \quad (5)$$

136 where the subscript is proper for the IGS TEC map product.  $C$  is a constant value of  $40.3 \text{ m}^3/\text{s}^2$ ,  $f$  is an appropriate frequency,  
 137 and  $VTEC$  is naturally the vertical total electron content in TECU units.  $N_e$  is electron density factor [electrons/ $\text{m}^3$ ], and  $h$  is  
 138 equal to the travelled ray path from the satellite to the rover. In turn,  $h_m$  is the height of the single layer of the ionosphere or  
 139 height of the piercing point for which the appropriate VTEC value from IGS TEC is interpolating. Hence, there is a need to  
 140 indicate the geodetic coordinates for ionospheric pierce point using e.g. geometric method formulation (Prol et al., 2017).

141 Taking into account ionospheric delay as a proportional value to TEC and proportional to the distance covered across  
 142 the band, the relation of VTEC and TEC can be defined (Leick et al., 2015):

$$143 \quad VTEC = \cos z' \cdot TEC \quad (6)$$

144 To integrate VTEC to STEC, the ionospheric mapping function, mentioned in the eq. (2) is presented as an inverse of the  
 145 cosines function. Note, the original sign  $z_k'$  was replaced by  $z_o'$  (Leick et al., 2015):

$$146 \quad F(z_o) = \frac{1}{\cos z'} = \left[ 1 - \left( \frac{R_e \sin z_o'}{R_e + h_m} \right)^2 \right]^{\frac{1}{2}} \quad (7)$$

147 where the adopted  $z'$  angle is equivalent to the zenith angle at the piercing point in (4).

148 Using eq. (5), (6), and (7), the ionospheric correction can be obtained in the ray path direction between satellite-rover:

$$149 \quad \delta_{IT} = \frac{40.3}{f^2} \cdot F(z_0) \cdot VTEC \quad (8)$$

150 Therefore, to briefly explain the mathematical model of SPP with utilized ionospheric corrections, the code observation  
 151 equation was adapted based on Strang and Borre (2008) with complementary changes:

$$152 \quad \begin{cases} P_r^s = \rho_r^s + c(\Delta t_r - \Delta t^s) + \delta_{TROP} + \delta_K + \varepsilon_p \\ P_r^s = \rho_r^s + c(\Delta t_r - \Delta t^s) + \delta_{TROP} + \delta_{IT} + \varepsilon_p \end{cases} \quad (9)$$

153 where the first equation is concerning on the SPP approach with Klobuchar algorithm and the second one is referring  
 154 to the IGS TEC map. The left side is the measured pseudo-range  $P_r^s$  between receiver  $r$  and satellite  $s$ . On the right side are  
 155 the model and estimated magnitudes: the geometrical distance  $\rho_r^s$  between receiver  $r$  and satellite  $s$  (position of the reference  
 156 station antenna used as a priori coordinates of receiver and satellite coordinates computed by utilization of the ephemeris  
 157 information), speed of light  $c$ , receiver and satellite clock biases:  $\Delta t_r$ ,  $\Delta t^s$ ,  $\delta_{TROP}$  tropospheric delay,  $\delta_K$  ionospheric delay  
 158 computed using Klobuchar algorithm (eight coefficients from navigation message) or  $\delta_{IT}$  - based on IGS TEC map utilizing  
 159 IONEX file and pseudo-range remaining error  $\varepsilon_p$ , respectively. In the research, the tropospheric corrections were obtained  
 160 based on Hopfield (see Hopfield, 1969) using model values of the dry and the wet subcomponents. Additionally, the clock  
 161 bias of satellites has been received by the utilization of satellites' ephemeris data and the relativistic improvements.

## 162 2.2 Modified SPP with autonomous VTEC estimation method

163 The essence of the proposed modified SPP method lies in an estimation of the  $\Delta VTEC$  term which is a variable  
 164 component of the ionospheric delay:

$$165 \quad \delta_{IONest} = \frac{40.3 \cdot 10^{16}}{f^2} \cdot F(z_0) \cdot (VTEC_0 + \Delta VTEC) \quad (10)$$

166 The modified SPP model with an independent method of the ionospheric effect estimation in the system of equations:

$$167 \quad \begin{cases} P_1 = \rho_r^{s_1} + c(\Delta t_r - \Delta t^{s_1}) + \delta_{TROP_1} + \delta_{IONest_1} + \varepsilon_1 \\ P_2 = \rho_r^{s_2} + c(\Delta t_r - \Delta t^{s_2}) + \delta_{TROP_2} + \delta_{IONest_2} + \varepsilon_2 \\ \cdot \\ \cdot \\ P_n = \rho_r^{s_n} + c(\Delta t_r - \Delta t^{s_n}) + \delta_{TROP_n} + \delta_{IONest_n} + \varepsilon_n \\ VTEC^{pseudoobs} = VTEC_0 + \Delta VTEC + \varepsilon_{\Delta VTEC} \end{cases} \quad (11)$$

168 The last row is a pseudo-observation equation in which  $VTEC_0$  is the constant, initial value of VTECs in a given epoch,



169 appropriate for all satellite elevation,  $\Delta VTEC$  is an estimated ingredient and  $\varepsilon_{\Delta VTEC}$  is a remaining error of determining factor. It  
 170 was decided, after performing many tests, to include this pseudo-observation equation into the SPP approach to ensure a  
 171 stable GPS solution. The model without the pseudo-observation formula would be too weak to give stable results (note that  
 172 single epoch positioning is used).

173 After many computational tests, it was assumed that the initial value of  $VTEC_0$  in any measured epochs during daytime  
 174 and nighttime of SPP is **5 TECU**. Therefore, the method does not need external information about VTEC referring to the  
 175 piercing point on the line of sight receiver – satellite, even if the IGS TEC map is available, it indicates that the model is  
 176 simple to build and implement into a complex algorithm. The reliability and usefulness will be submitted during the  
 177 presentation of the results.

178 It is assumed in this method that the “observed” and approximate values are equal:

$$179 \quad VTEC^{pseudoobs} = VTEC_0 \quad (12)$$

180 Continuing, to simplify successive descriptions of the modified SPP approach, the mapping coefficient is denoted:

$$181 \quad mapcoeff = \frac{40.3 \cdot 10^{16}}{f^2} F(z_0) \quad (13)$$

182 The system of code equations (11) after linearization can be introduced in the matrix notation with covariance matrix:

$$183 \quad \mathbf{e} = \mathbf{Ax} - \mathbf{y}, \quad \mathbf{C}_x = m_0^2 \mathbf{W}^{-1} \quad (14)$$

184 where:

$$185 \quad \mathbf{e} = \begin{bmatrix} -\varepsilon_1 \\ \vdots \\ -\varepsilon_n \end{bmatrix} \quad (15)$$

186 is a residual vector of theoretical corrections,

$$187 \quad \mathbf{A} = \left[ \begin{array}{ccc|c|c} a_{11} & a_{12} & a_{13} & 1 & mapcoeff^1 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ a_{n1} & a_{n2} & a_{n3} & 1 & mapcoeff^n \\ \hline 0 & 0 & 0 & 0 & 1 \end{array} \right] \quad (16)$$

188 is a design matrix. The first three columns in first block contains derivatives values from Taylor’s series, based on satellite  
 189 coordinates in the specified epochs ( $i$ ), approximate rover coordinates ( $r_0$ ) and geometrical distance between rover and

190 satellite:  $a_{i1} = -\frac{X' - X_m}{\rho_m^i}, a_{i2} = -\frac{Y' - Y_m}{\rho_m^i}, a_{i3} = -\frac{Z' - Z_m}{\rho_m^i}$ , respectively. The last column in the first block, relates to the clock error in

191 meters.

192 The vector of unknowns receives an additional parameter in the adjustment process:

$$193 \quad \mathbf{x} = \begin{bmatrix} \Delta X_r \\ \Delta Y_r \\ \Delta Z_r \\ c\Delta t_r \\ \hline \Delta VTEC \end{bmatrix} \quad (17)$$

194 The disclosure vector is:

$$195 \quad \mathbf{y} = \begin{bmatrix} y_r^1 \\ \vdots \\ y_r^n \\ \hline 0 \end{bmatrix} \quad (18)$$

196 where  $y_r^i = P_i - \rho_i^r + c\Delta t^i - \delta_{TROP_i} - mapcoeff \cdot VTEC_0$ . The last entry amounts to zero because of assumption (12).

197 The weight matrix has been prepared based on pseudo-range measurement error which was assumed as a 2.00 m and  
 198 appropriate satellite elevation angle. The criterion of the minimal mask was implemented as a 10 degree. After  
 199 computational tests with theoretical analysis, the weight of the estimated component  $\Delta VTEC$  was assumed in the model as 1.

$$200 \quad \mathbf{W} = \begin{bmatrix} \frac{1}{\delta^2} \sin(elev_1) & \dots & 0 & \vdots & 0 \\ \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & \dots & \frac{1}{\delta^2} \sin(elev_n) & \vdots & 0 \\ \hline 0 & \dots & 0 & 0 & 1 \end{bmatrix} \quad (19)$$

201 The least-squares estimate of the equation (14) is computed from the normal equations together with its covariance  
 202 matrix with the variance factor:  $m_0^2 = \frac{\mathbf{e}^T \mathbf{W} \mathbf{e}}{n - m}$ . The number of parameters  $m = 5$ . Thus, the minimal number of observations  
 203 should be  $n = 6$  to ensure necessary redundancy.

### 204 2.3 Accuracy analysis criteria

205 The basic statistical operator in the experiment is a distance of the solution from the true position *dist* where subscript  
 206 “r” means calculated rover’s coordinates and “t” regarding to the actual position. Moreover, its average value (*DIST*),  
 207 computed from solutions obtained from the single epochs with its mean error. The actual position means constant station  
 208 coordinates provided by the agency, which manage the Continuously Operating Reference Station (CORS) used in the  
 209 experiment for evaluation of the positioning model accuracy. The formula can be introduced in each epoch in the form of  
 210 Euclidean distance:

211  $dist_{ep_i} = \sqrt{(X_r - X_t)^2 + (Y_r - Y_t)^2 + (Z_r - Z_t)^2}$  (20)

212 The formula to calculate the mean error of average solution is as follows:

213  $m_{dist_{ep_i}}^2 = \mathbf{GC}_{\hat{\mathbf{x}}_{ep_i}} \mathbf{G}'$  (21)

214 where  $\mathbf{C}_{\hat{\mathbf{x}}}$  is a covariance matrix of the parameter vector and  $\mathbf{G}$  is a gradient:

215  $\mathbf{G} = \begin{bmatrix} \frac{\Delta X_{ep_i}}{dist_{ep_i}} & \frac{\Delta Y_{ep_i}}{dist_{ep_i}} & \frac{\Delta Z_{ep_i}}{dist_{ep_i}} \end{bmatrix}$  (22)

216 where  $\Delta X_{ep_i}$ ,  $\Delta Y_{ep_i}$ ,  $\Delta Z_{ep_i}$  are the coordinates differences between calculated rover position ( $r$ ) and the appropriate actual  
217 position of reference station ( $t$ ),  $dist_{ep_i}$  are explained in formula (20). The average value is as follows:

218  $m_{DIST}^2 = \frac{1}{n^2} \sum_{i=1}^n m_{dist_{ep_i}}^2$  (23)

219 The NEU (North East Up) coordinates system was used in the comparative analysis, where the calculated rover's  
220 position is compared to the actual position. Therefore, the rotation matrix was used to convert the covariance matrix (14) of  
221 the parameters to the NEU system:

222  $\mathbf{C}_{NEU} = \mathbf{RC}_{\hat{\mathbf{x}}}\mathbf{R}^T$  (24)

223 where:

224  $\mathbf{R} = \begin{bmatrix} -\sin\varphi\cos\lambda & -\sin\varphi\sin\lambda & \cos\varphi \\ -\sin\lambda & \cos\lambda & 0 \\ \cos\varphi\cos\lambda & \cos\varphi\sin\lambda & \sin\varphi \end{bmatrix}$  (25)

225 The  $\varphi$  and  $\lambda$  are rover geodetic coordinates.

226 The covariance matrix of mean values computed from the whole observational day is:

227  $\mathbf{C}_{NEU_{mean}} = \mathbf{DC}_{NEU_{set}}\mathbf{D}^T = \frac{1}{n^2} \sum_{i=1}^n \mathbf{C}_{NEU_{ep_i}}$  (26)

228 where  $\mathbf{C}_{NEU_{set}}$  is a block matrix which contains on the diagonal the covariance matrixes in the NEU setup from all measured  
229 epochs ( $n$ ) and  $\mathbf{D}$  is treated as a transition matrix from the NEU to their mean values:

$$\mathbf{D} = \begin{bmatrix} \frac{1}{n} & 0 & 0 & \frac{1}{n} & 0 & 0 & \dots & \frac{1}{n} & 0 & 0 \\ 0 & \frac{1}{n} & 0 & 0 & \frac{1}{n} & 0 & \dots & 0 & \frac{1}{n} & 0 \\ 0 & 0 & \frac{1}{n} & 0 & 0 & \frac{1}{n} & \dots & 0 & 0 & \frac{1}{n} \end{bmatrix} \quad (27)$$

### 231 3 Numerical experiment and discussion

232 In this section, the explanation of the research concept will be done. Next, the appropriate numerical experiment in  
 233 view of graphics and numeric settings. The parallel discussion about obtained results for appropriate interpretation will be  
 234 made.

#### 235 3.1 Research concept

236 The numerical experiment is based on real single frequency code pseudorange observations from Global Positioning  
 237 System (GPS). Namely, C1C code data on the L1 carrier frequency (1575.42 MHz). Continuing, three different EURE  
 238 Permanent GNSS Network stations have been chosen in Scandinavia. Two stations in Sweden – Visby (VIS) and Skellefteå  
 239 (SKE), one in Norway – Vardø (VAR). The observational files and initial coordinates of receivers was gained from the  
 240 BKG (Bundesamt für Kartographie und Geodäsie) GNSS Data Center. The parameters of satellite orbits (SP3 file) and  
 241 atmospheric data were obtained by means of CDDIS (Crustal Dynamics Data Information System) - in fact, IONEX  
 242 (IONosphere map EXchange format) only in view of atmospheric data, as a source of IGS TEC map. The coordinates of  
 243 points were treated as the true coordinates in the practical part of the experiment. The reference coordinates are presented in  
 244 the table:

245 **Table 1.** Actual coordinates of points

Points	X	Y	Z
VIS600SWE	3246466.556	1077901.829	5365279.606
SKE800SWE	2534032.877	9751679.370	5752078.718
VAR500NOR	1844607.623	1109719.107	5983936.007

246  
 247 In the models, the actual coordinates have been converted to the antenna phase center to make a comparative analysis with  
 248 the SPP results, where measurements were executed to the antenna phase center.

249 Three different localizations allow checking how the modified SPP model works on different geodetic latitude because  
 250 of ionosphere activity changes, so its quality in the GPS code domain can be widely stated.

251 The research concept focuses on measurement on two different days in the cited locations. Therefore, three stations of  
 252 the EUREF Permanent GNSS Network were employed for comparative analysis based on data from two parallel days.

253 **Table 2.** Experiment concept

Points	Days	SPP approaches
VIS	15/06/2019	SPP with Klobuchar algorithm (SPPwithKM)
	15/08/2019	Modified SPP with Vertical Total Electron Content estimation (MSPPwithdVTEC)
SKE	15/06/2019 15/08/2019	SPP with IGS TEC map (SPPwithITM)
		SPP with Klobuchar algorithm (SPPwithKM)
		Modified SPP with Vertical Total Electron Content estimation (MSPPwithdVTEC)
VARS	15/06/2019 15/08/2019	SPP with IGS TEC map (SPPwithITM)
		SPP with Klobuchar algorithm (SPPwithKM)
		Modified SPP with Vertical Total Electron Content estimation (MSPPwithdVTEC)
		SPP with IGS TEC map (SPPwithITM)

254 To execute the numerical experiment of the research , the MATLAB environment from The MathWorks was used. The  
 255 “PostCalc” software developed by Dawid Kwaśniak was utilized as the base MATLAB program. Next, the complementary  
 256 changes were done by the authors of manuscript due to numerical experiment requirement..

### 257 3.2 Discussion of the experiment results

258 The Figures 1-3 present the distribution of *dist* values during the observational day (*Results of the positioning models*)  
 259 and their average value *DIST* with appropriate mean errors in the middle (*Average results of the positioning models*). In turn,  
 260 the bottom parts show the error reduction of the models (*Differences of the positioning models*). The upper part of  
 261 Figure 1(a) demonstrates the solutions for Visby station on 15 June, 2019. The *dist* results are significantly improved for  
 262 **MSPPwithdVTEC** referring to the **SPPwithKM** what is confirmed by the average value of *DIST* equalled to 4.886 m.  
 263 There is not a major difference of *DIST* between **MSPPwithdVTEC** and **SPPwithITM** (0.033 m). Therefore, the mean error  
 264 of *DIST* (0.072 m) affirms the precision of the modified solution. Studying the bottom division of Figure 1(a), **SPPwithKM**  
 265 was assumed as a reference one (100%) in the calculation of the percent values of error reduction based on *DIST*. The results  
 266 are satisfying because of error reduction on the level of 22.97% in the **MSPPwithdVTEC** case and the close discrepancy  
 267 with the error reduction of the **SPPwithITM** (0.53%). The second day using Visby station is 15 August, 2019. In the middle  
 268 of Figure 1(b), *DIST* is beneficial for the **MSPPwithdVTEC** (4.912 m) compared to the reference model which leads to  
 269 defining the tendency of improved accuracy in the SPP. Again, the difference in the average solutions of *DIST* between  
 270 **MSPPwithdVTEC** and **SPPwithITM** is insignificant (0.055 m) according to code observations accuracy level. Thus, the  
 271 accuracy of the estimation method is comparable with the IGS TEC map. Focusing on the average explanation of the *DIST*  
 272 mean errors among the **MSPPwithdVTEC** (0.067 m) and the **SPPwithITM** (0.074 m), these approaches do not distinctly  
 273 vary, which indicates that the proposed SPP model works well. In the bottom of Figure 1(b), the error reduction of  
 274 **MSPPwithdVTEC** is 20.90% and is at a similar level with **SPPwithITM** (21.79%). The **SPPwithKM** proved to be the  
 275 lowest accuracy method. Probably, the ionospheric corrections obtained by the coefficients from the navigation message  
 276 cannot reflect the changes that take place in the ionosphere with the higher temporal accuracy. Briefly, in the first studied  
 277 point, the **MSPPwithdVTEC** can be judged as the precise SPP model.

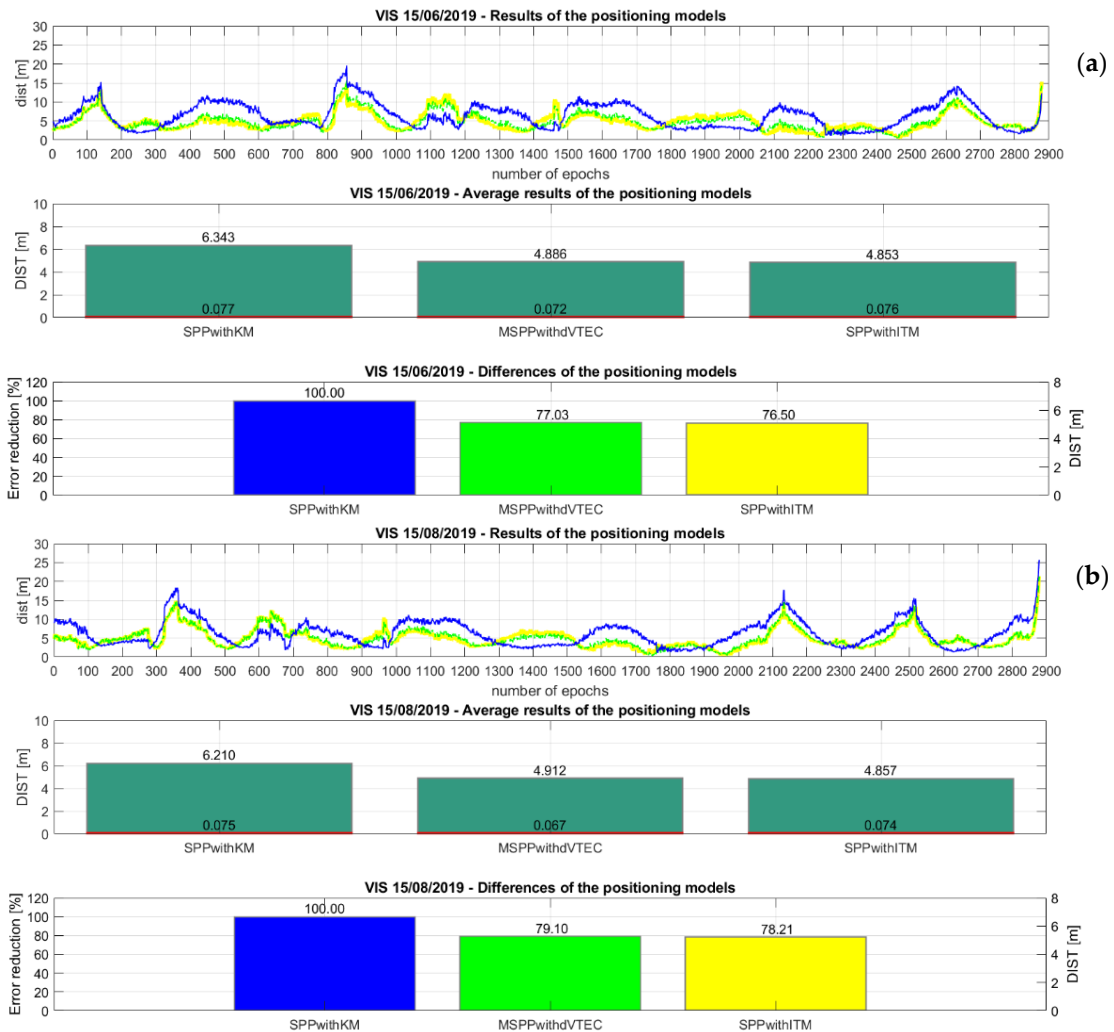
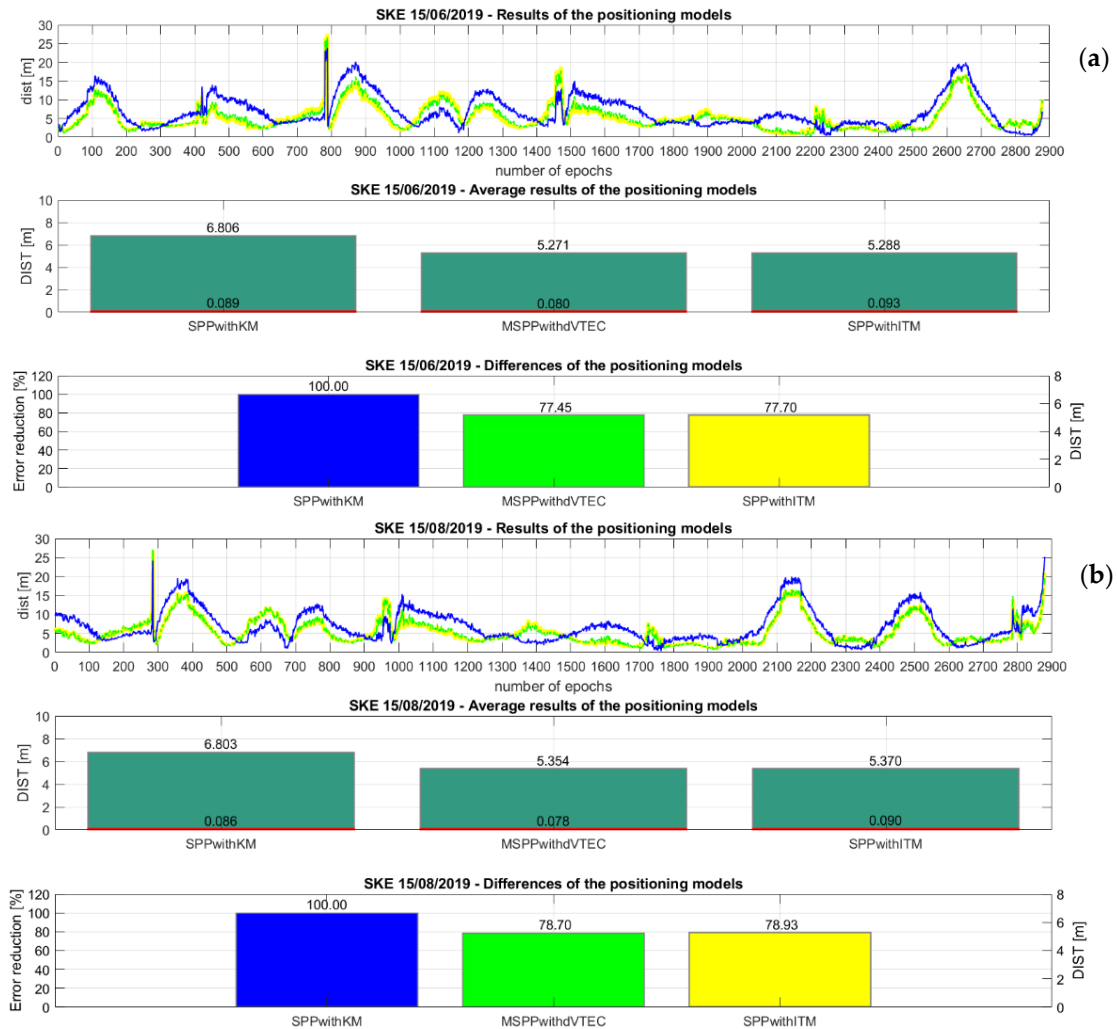


Figure 1. Set of the results of the positioning models: (a) VIS 15/06/2019 (b) VIS 15/08/2019

Following the experiment report, the next examined subject is SKE 15/06/2019. Looking at Figure 2(a), the top part presents the *dist* distribution of the **MSPPwithdVTEC** solutions close to the **SPPwithITM**. The average description of *DIST* validates this declaration, where the difference between these two approaches is 0.017 m, in favor of the **MSPPwithdVTEC**. In turn, according to the base model, the **MSPPwithdVTEC** delivers solutions with highly-increased accuracy, which is the most important. Despite such accuracy, the *DIST* precision of **MSPPwithdVTEC** (0.080 m) is improved and is at a similar level as **SPPwithITM** (0.093 m), which confirms the consistency of the methods. Explaining the bottom part of Figure 2(a), the error reduction of the **MSPPwithdVTEC** is at the beneficial level of 22.55%, which is again close to the reduction obtained by **SPPwithITM** (22.30%). Therefore, this method can be evaluated as the approach of a similar class compared to the case with IGS TEC map. The second day of tests is 15 August 2019. Based on *dist* in the top of Figure 2(b), it is noticeable that the **MSPPwithdVTEC** results are at related relatively similar level as **SPPwithITM**.

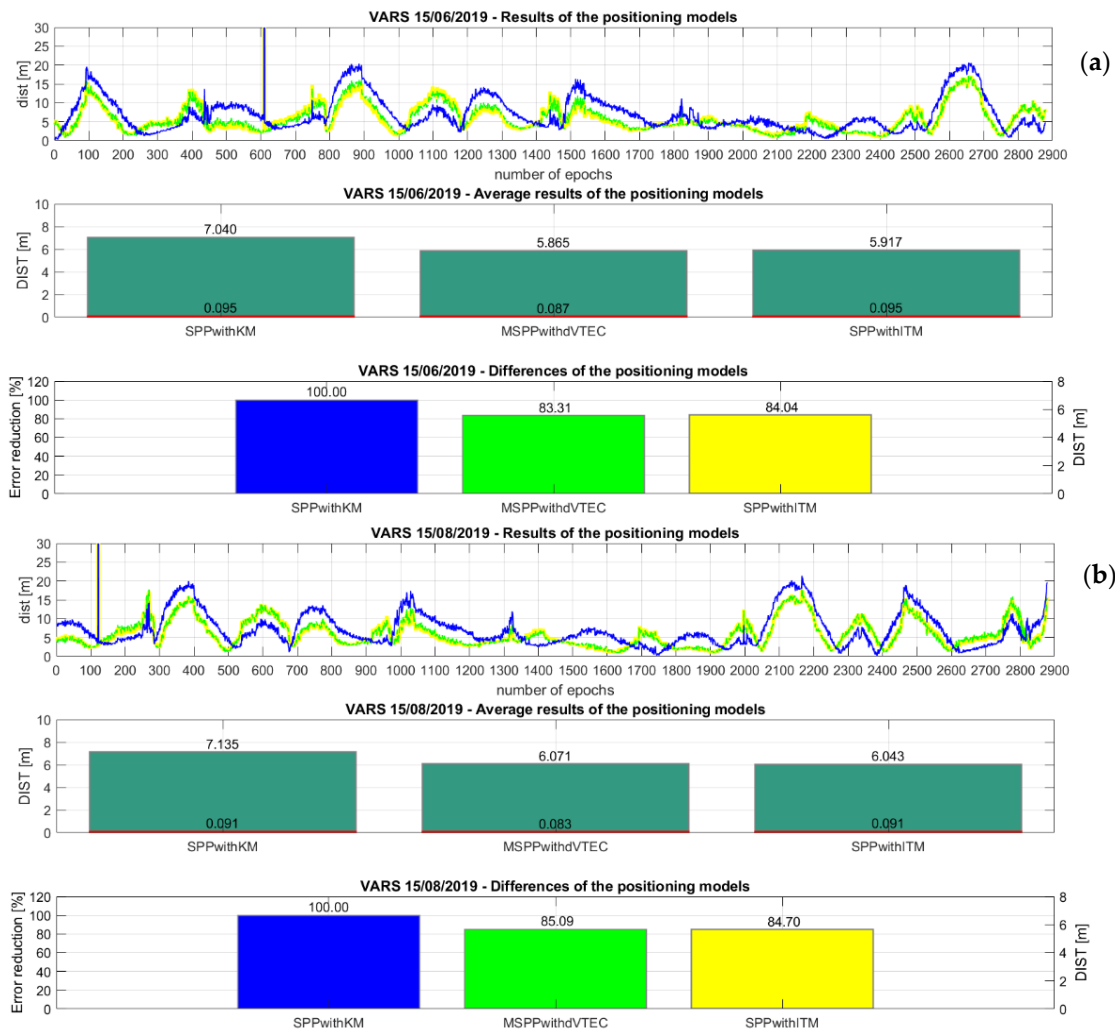
311 Looking in the middle part of Figure 2(b), the increased accuracy in **MSPPwithdVTEC** is verified by the *DIST* solution  
 312 equal to 5.354 m, referring to the initial **SPPwithKM**. The mean error of *DIST* gives an acceptable value using  
 313 **MSPPwithdVTEC** by comparable magnitude with the other models. Considering the bottom part of Figure 2(b), the error  
 314 reduction amounts to 21.30% whereas the approach with the IGS TEC map achieves an equivalent value of 21.07%. In sum,  
 315 the **MSPPwithdVTEC** can be assessed on the next EUREF's location as the valuable SPP approach by use of the new  
 316 method of the ionospheric refraction estimation, without the need for external products, e.g. atmospheric factors or GIMs.



334 **Figure 2.** Set of the results of the positioning models: (a) SKE 15/06/2019 (b) SKE 15/08/2019

335 The last studied point is VARS00NOR. The first examined day is 15 June 2019. The middle part of Figure 3(a)  
 336 demonstrates that the *DIST* difference of the two approaches: **SPPwithITM** and **MSPPwithdVTEC** is 0.052 m, therefore  
 337 the improved accuracy is at a similar level, referring to **SPPwithKM** average observations. The precision of *DIST* confirms

338 the reliability of the **MSPPwithdVTEC**, where the mean error is equal to 0.087 m with an insignificant discrepancy  
 339 (0.008 m) compared to the **SPPwithITM**. The bottom part of Figure 3(a) shows a decrease in the percent value of the error.  
 340 The error reduction of the **MSPPwithdVTEC** is at the level of 16.69%, thus the improvement of accuracy is verified. Again,  
 341 the difference of error reduction among **MSPPwithdVTEC** and **SPPwithITM** is on the parallel level (0.73%) which  
 342 confirms the method credibility. The second tested day, and therefore the last one, is 15 August 2019. The *DIST* elaboration  
 343 in Figure 3(b) presents the low differences between the two principal approaches on the level of 0.028 m. Studying the  
 344 bottom division of Figure 3(b), the **MSPPwithdVTEC** achieves a positive level of error reduction of 14.91%, relating to the  
 345 **SPPwithKM**. In addition, the top parts of Figure 3 (a) and (b) present the distribution of **MSPPwithdVTEC** *dist* results as  
 346 close in value to the **SPPwithITM** with increased accuracy to **SPPwithKM**. This finding is also valid to other examined  
 347 cases. Thus, the proposed model can be identified as stable and accurate. The error reduction is at a satisfactory level.  
 348



367 **Figure 3.** Set of the results of the positioning models: (a) VARS 15/06/2019 (b) VARS 15/08/2019



368 Focusing on the mean errors of the final solution in the NEU system, we will consider the average precision of the  
 369 differences of the components  $\Delta N$ ,  $\Delta E$ , and  $\Delta U$ , referring to the daily result. The difference means the discrepancy between  
 370 the actual station's coordinates and the received position from the SPP methods. For this purpose, the Eq. (28) was used to  
 371 determine the mean values of  $\Delta N$ ,  $\Delta E$  and  $\Delta U$  errors which are summarized in the table below:

372 **Table 3.** Average errors of the difference in the positions using the NEU system

<b>SPP approaches</b>	<b><math>m_{\Delta N}</math></b>	<b><math>m_{\Delta E}</math></b>	<b><math>m_{\Delta U}</math></b>	<b>Stations and Days</b>
SPPwithKM	0.06	0.04	0.10	VIS 15/06/2019
<b>MSPPwithdVTEC</b>	<b>0.05</b>	<b>0.04</b>	<b>0.09</b>	
SPPwithITM	0.06	0.04	0.09	
SPPwithKM	0.06	0.04	0.09	VIS 15/08/2019
<b>MSPPwithdVTEC</b>	<b>0.06</b>	<b>0.03</b>	<b>0.08</b>	
SPPwithITM	0.06	0.04	0.09	
SPPwithKM	0.05	0.03	0.11	SKE 15/06/2019
<b>MSPPwithdVTEC</b>	<b>0.04</b>	<b>0.03</b>	<b>0.10</b>	
SPPwithITM	0.05	0.03	0.11	
SPPwithKM	0.05	0.03	0.11	SKE 15/08/2019
<b>MSPPwithdVTEC</b>	<b>0.04</b>	<b>0.03</b>	<b>0.10</b>	
SPPwithITM	0.05	0.03	0.11	
SPPwithKM	0.04	0.03	0.11	VARS 15/06/2019
<b>MSPPwithdVTEC</b>	<b>0.04</b>	<b>0.03</b>	<b>0.10</b>	
SPPwithITM	0.04	0.03	0.11	
SPPwithKM	0.04	0.03	0.11	VARS 15/08/2019
<b>MSPPwithdVTEC</b>	<b>0.04</b>	<b>0.03</b>	<b>0.10</b>	
SPPwithITM	0.04	0.03	0.11	

373 The error quantities of the difference in the positions were achieved for **MSPPwithdVTEC** and **SPPwithITM** on a  
 374 close level. Separating the horizontal and the vertical components of the position, the **MSPPwithdVTEC** is characterized by  
 375 comparable precision to **SPPwithKM** in the North and East direction, therefore, the additional estimated parameter in the  
 376 code equation does not change the SPP model enough to reduce its quality. The case is repeated in the context of the vertical  
 377 component U. The **MSPPwithdVTEC** is profitable and achieves the similar values of the mean errors to **SPPwithITM**. In  
 378 general, the values are close to each other and the differences are not as clear in the context of the code data use. Therefore,  
 379 the quantities of average errors demonstrate that **MSPPwithdVTEC** is the approach of the closest precision to the  
 380 **SPPwithITM**, specified as a high-quality product, which is the most important from the authors' point of view.  
 381

#### 382 4 Conclusions and future perspectives

383 The main idea of this paper was to introduce the new method to estimate the ionospheric delay in the SPP without using  
 384 the external data. Moreover, in the case of comparative analysis, two common approaches in SPP was employed: SPP with  
 385 Klobuchar algorithm and SPP with IGS TEC map. The first one was treated as a reference one. The SPP model with IGS

386 TEC map was utilized to authenticate the proposed model in view of IGS TEC map use - defined as a high-quality product.  
387 The explanation of mathematical models and appropriate accuracy analysis criteria was done. Next, the numerical  
388 experiment using real code data from three different GNSS stations with discussion to interpret the obtained results.  
389 Referring to achieved solutions, the proposed approach can be defined as a simple and independent way to improve SPP.  
390 Moreover, the **MSPPwithdVTEC** can be employed in the procedure of determination the approximate position for the need  
391 of the single-epoch precise positioning.

392 Based on the mean distance of the solution from the true position, the **MSPPwithdVTEC** achieved improved GPS  
393 position in comparison to the basic **SPPwithKM** in each tested station. Moreover, the **MSPPwithdVTEC** acquires a similar  
394 level of error reduction to the **SPPwithITM** what is the most satisfying in view of method authentication.

395 Finally, the results of the **MSPPwithdVTEC** confirm the potential use of the mathematical model in the SPP. The  
396 strategy should be developed in the future through the verification of model stability in the other stations since ionosphere  
397 changes are highly dependent on localization. Therefore, the proposed method of SPP can be recognized as a good forecast  
398 to become independent of external products delivering information about the ionospheric delay.

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401

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