



## Daedalus Ionospheric Profile Continuation (DIPCont)

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**Abstract.** The Daedalus Ionospheric Profile Continuation (DIPCont) project is concerned with the question how in situ measurements in the lower thermosphere and ionosphere (LTI) can be extrapolated using parametric models of observables and derived variables. To reflect the pronounced change of temperature across the LTI, non-isothermal models for neutral density and also electron density are constructed from scale height profiles that increase linearly with altitude. Ensembles of model parameters are created by means of Monte Carlo simulations using synthetic measurements based on model predictions and relative uncertainties as specified in the Daedalus Report for Assessment. The parameter ensembles give rise to ensembles of model altitude profiles for LTI variables of interest. Extrapolation quality is quantified by statistics derived from the altitude profile ensembles. The vertical extent of meaningful profile continuation is captured by the concept of extrapolation horizons defined as the boundaries of regions where the deviations remain below a prescribed error threshold. The methodology allows for assessing how cost-critical elements of the Daedalus mission proposal such as perigee and apogee distances as major factors controlling the necessary amount of propellant and radiation shielding, respectively, affect the accuracy of scientific inference in the LTI. First results are presented for dual-satellite measurements at different inter-spacecraft distances but also for the single-satellite case to compare the two basic mission scenarios under consideration. DIPCont models and procedures are implemented in a collection of Python modules and Jupyter notebooks supplementing this report.

### 15 1 Introduction

The lower thermosphere and ionosphere (LTI) at altitudes between about 100 km and 200 km is characterized by transitions of several atmospheric attributes. It is the lower part of the heterosphere where atmospheric constituents are no longer mixed by turbulence, and start to follow separate barometric laws (e.g., Picone et al., 2002; Izakov, 2007). As part of the thermosphere, the temperature profile shows a significant increase with altitude throughout the whole LTI (e.g., Chamberlain and Hunten, 1987). As part of the ionosphere, it includes the E-layer peak in electron density and the bottom side of the F-layer (e.g., Hargreaves, 1992). With strongly altitude-dependent neutral-ion and neutral-electron collision frequencies, the LTI supports

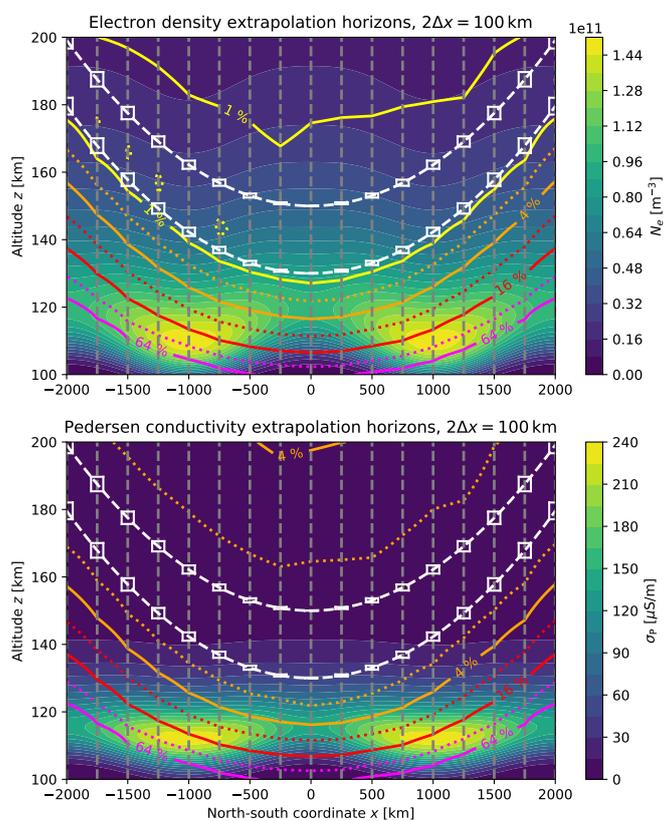


an anisotropic conductivity tensor that gives rise to a complex interplay of electric fields and currents. The conductivity tensor components affecting the directions perpendicular to the ambient magnetic field, namely, Pedersen and Hall conductivities, show pronounced maxima in the LTI (e.g., Baumjohann and Treumann, 1996). A key variable quantifying its energetics is the  
25 Joule heating rate. Particular rich dynamics can be observed in the auroral region at high latitudes where energy and momentum from the magnetosphere are fed into the ionosphere through currents flowing parallel to the ambient magnetic field lines (e.g., Vogt et al., 1999). A comprehensive review of LTI features, measurement techniques, and models is provided by Palmroth et al. (2021).

Since the early 20th century, the LTI has been studied extensively using ground-based remote sensing facilities such as  
30 ionosondes and radars, but in all aspects requiring in-situ observations it remains underexplored territory. Rocket flights (e.g., Sangalli et al., 2009) can offer only local and temporally confined information. Major technical challenges have so far prevented a satellite mission to the deep, dense part of the LTI, despite scientific interest, community proposals, and feasibility studies by major space agencies. A recent initiative along this line is the Daedalus mission proposal (Sarris et al., 2020), submitted to  
35 for a Phase-0 science and technical study. The Daedalus Report for Assessment (ESA, 2020) includes a thorough review of key LTI variables, like neutral density and temperature, electron density, and conductivities.

The *Daedalus Ionospheric Profile Continuation (DIPCont)* project is concerned with vertical profiles of LTI variables and their reconstruction from dual-spacecraft and single-spacecraft observations. More specifically, the focus of the project is on the *quality* of profile continuation towards the lower LTI with its maxima in conductivities and current intensities, as given  
40 by the accuracy, the resolution, and the coverage of the reconstructions obtained from in-situ measurements. Inspired by early work to extrapolate vertical profiles carried out under the Daedalus Phase-0 Science Study, DIPCont introduces a systematic probabilistic approach to the problem.

Using the parametric models of key LTI observables and derived variables described in Section 2, representative ensembles of altitude profiles are generated by means of Monte Carlo simulations as explained in Section 3. The altitude profile ensembles  
45 give rise to statistical measures of relative deviation which in turn allow for estimating extrapolation horizons, effectively capturing the altitude range where deviations remain within given error thresholds. The basic ideas are illustrated in Figure 1, displaying the extrapolation horizons for a range of relative error thresholds on top of the model distributions of electron density and Pedersen conductivity used for producing synthetic measurements along the orbits of a dual-satellite mission. Further first results are presented in Section 4, including a brief comparison between the single-spacecraft and the dual-spacecraft scenario.  
50 In Section 5, our findings are discussed in the context of important technical parameters and constraints relevant for a low-altitude mission. The body of the paper is concluded in Section 6 with prospects for upcoming work. Model derivations and technical details are presented in the Appendices, with particular emphasis on the incorporation of a non-isothermal temperature profile varying linearly with altitude.



**Figure 1.** Two-dimensional section of the modeled LTI. Upper panel: Electron density  $N_e$ . Lower panel: Pedersen conductivity  $\sigma_p$ . Synthetic measurements are produced along the two satellite orbits (white dashed lines). The parameters of vertical profiles are estimated using measurements within a window (white solid rectangle) of width  $2\Delta x$  around the nodes of a horizontal grid (gray dashed lines). Extrapolation horizons (solid and dotted colored lines) for a set of relative error levels are displayed as contours of a relative deviation measure, here the root-mean-square deviation of the ensemble of extrapolated profiles from the synthetic model prediction.



## 2 Parametric models of LTI variables

55 In this first version of the DIPCont model, the LTI is described by a series of self-consistent parametric models to assess the quality of conductivity profile reconstruction from in situ measurements. Considering Pedersen conductivity for a quasi-neutral two-component plasma and disregarding the contribution from electron-neutral collisions, the expression

$$\sigma_P = \frac{N_e e^2}{m_i} \frac{\nu_{in}}{\nu_{in}^2 + \Omega_i^2} \quad (1)$$

( $e$ : elementary charge,  $m_i$ : ion particle mass) suggests that the altitude variabilities of electron number density  $N_e$  and ion-neutral collision frequency  $\nu_{in}$  need to be modeled carefully. Less critical is the ion gyrofrequency  $\Omega_i$  as it does not vary much over the LTI altitude range, and is captured with sufficient accuracy by well-established empirical models. Different parametrizations exist for the ion-neutral collision frequency  $\nu_{in}$  (e.g., Palmroth et al., 2021; Huba, 2019; Evans et al., 1977). In general the expressions are directly proportional to the number density  $N_n$  of neutral particles.

Altitude profiles of neutral density  $N_n$  and electron density  $N_e$  depend on neutral temperature  $T_n$ . While isothermal approximations are still widely used for sufficiently narrow atmospheric layers, pronounced temperature changes over the LTI altitude range require at least a simplified non-isothermal description. Below we consider a linear temperature profile capturing a representative range of typical thermospheric values (Picone et al., 2002) that in the LTI can be seen as an approximation of the classical thermospheric profile suggested by Bates (1959) as a solution of the heat conduction equation. Self-consistent parametric models of neutral density  $N_n$  and electron density  $N_e$  are developed for the linear temperature profile.

70 Note the model functions are *local representations* of altitude profiles in the sense that they refer to a flexible reference altitude,  $z_0$ , that can be adapted to the locations where measurements are taken. In the DIPCont development phase it was observed that parameters of model functions in local representations typically showed weaker correlations and could be estimated more reliably, in particular as compared to the *regional representations*, relying on parameters at some fixed altitude, like the peak electron density height.

75 As in the Daedalus Report for Assessment (ESA, 2020), the vertical boundaries of the LTI region are assumed to be at  $z_B = 100$  km (base or bottomside altitude) and  $z_T = 200$  km (topside altitude).

### 2.1 Neutral temperature

Neutral temperature  $T_n$  is assumed to vary linearly with altitude  $z$ :

$$T_n(z|z_0, T_{n0}, L_{n0}) = T_{n0} \cdot \left(1 + \frac{z - z_0}{L_{n0}}\right). \quad (2)$$

80 The parameters  $T_{n0}$  and  $L_{n0}$  are the neutral temperature and the gradient length scale, respectively, at a reference altitude  $z_0$ . The constant temperature gradient is given by

$$\frac{dT}{dz} = \frac{T_{n0}}{L_{n0}}. \quad (3)$$



## 2.2 Scale height parameters

The pressure scale height  $H_n^P$  is defined as

$$85 \quad H_n^P = \frac{kT_n}{m_n g} = \frac{R_{\text{gas}} T_n}{M_n g} \quad (4)$$

where  $k$  is the Boltzmann constant,  $g$  is gravitational acceleration,  $R_{\text{gas}}$  is the universal gas constant,  $m_n$  is the average particle mass, and  $M_n$  is the average molar mass. Disregarding altitude changes of atmospheric composition and gravity, the height variation of pressure scale height is also linear which in turn means that the gradient of pressure scale height

$$\frac{dH_n^P}{dz} = \frac{R_{\text{gas}}}{M_n g} \frac{dT_n}{dz} = \frac{R_{\text{gas}}}{M_n g} \frac{T_{n0}}{L_{n0}} \quad (5)$$

90 is constant. In Appendix A it is shown that this invariance implies that also the density scale height  $H_n^N$  varies only linearly, and the constant inverse gradients

$$\gamma = \left( \frac{dH_n^P}{dz} \right)^{-1} \quad (6)$$

and

$$\eta = \left( \frac{dH_n^N}{dz} \right)^{-1} \quad (7)$$

95 are related through

$$\eta = \gamma + 1. \quad (8)$$

According to Eq. (A11), the local density scale height  $H_{n0}^N$  can be obtained from

$$\begin{aligned} H_{n0}^N &= \frac{H_{n0}^P}{1 + \gamma^{-1}} = \frac{\gamma}{\gamma + 1} H_{n0}^P = \frac{\eta - 1}{\eta} H_{n0}^P \\ &= \frac{\eta - 1}{\eta} \frac{R_{\text{gas}} T_{n0}}{M_n g}. \end{aligned} \quad (9)$$

100 Using Eq. (A13), the neutral temperature profile can be expressed by means of the parameters  $\eta$  and  $H_{n0}^N$  as follows:

$$T_n(z|z_0, T_{n0}, H_{n0}^N, \eta) = T_{n0} \cdot \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right). \quad (10)$$

In the LTI, the temperature varies significantly with altitude, latitude, and season (Picone et al., 2002). As reference values we adopt  $T_{nB} \sim 200$  K at  $z_B = 100$  km, and  $T_{nT} \sim 1000$  K at  $z_T = 200$  km, hence  $dT/dz \sim 8$  K/km, and  $L_{nB} \sim 25$  km. At  $z_B$ , the pressure scale height is  $H_{nB}^P \sim 6$  km, thus  $H_{nB}^P/L_{nB} \sim 0.24$ . This gives  $\gamma \sim 4$ ,  $\eta \sim 5$ , and  $H_{nB}^N \sim 5$  km for the density scale height at the base of the LTI.



### 2.3 Neutral density

The altitude dependence of neutral density  $N_n$  for linear scale height profiles is derived in Appendix A, resulting in the following local representation

$$\begin{aligned} N_n(z|z_0, N_{n0}, H_{n0}^N, \eta) &= N_{n0} \cdot \exp \left\{ -\eta \ln \left( 1 + \frac{z-z_0}{\eta H_{n0}^N} \right) \right\} \\ &= N_{n0} \cdot \left( 1 + \frac{z-z_0}{\eta H_{n0}^N} \right)^{-\eta}, \end{aligned} \quad (11)$$

110 see also Eq. (A15). The parameter  $N_{n0} = N_n(z_0)$  is the local neutral density, i.e., its value at the reference altitude  $z_0$ .

### 2.4 Electron density

The altitude dependence of electron density  $N_e$  for linear scale height profiles is derived in Appendix B, resulting in the following local representation

$$\begin{aligned} N_e(z|z_0, N_{e0}, L_{r0} \cos \chi, H_{n0}^N, \eta) &= N_{e0} \exp \left\{ \frac{1}{2} \frac{\eta}{\eta-1} \left[ -\theta_0 + \frac{H_{n0}^N}{L_{r0} \cos \chi} (1 - e^{-\theta_0}) \right] \right\} \end{aligned} \quad (12)$$

115 with  $\theta_0 = \theta_0(z) = (\eta - 1) \ln \left( 1 + \frac{z-z_0}{\eta H_{n0}^N} \right)$ , see Eq. (B16). The parameter  $N_{e0} = N_e(z_0)$  gives electron density at the chosen reference altitude  $z_0$ . Note that  $L_{r0}$  and  $\chi$ , the angle of incident radiation with the atmospheric layer normal direction, cannot be estimated separately but only combined as  $L_{r0} \cos \chi$ . The parameters  $H_{n0}^N$  and  $\eta$  can be inherited from estimations using neutral temperature and/or neutral density data, effectively reducing the number of electron density parameters and thus stabilizing the estimation procedure.

120 The non-isothermal electron density model can also be expressed in terms of the ionization peak parameters, namely, the altitude  $z_*$  and the electron density value  $N_{e*} = N_e(z_*)$ :

$$\begin{aligned} N_e(z|z_*, N_{e*}, H_{n*}^N, \eta) &= N_{e*} \exp \left\{ \frac{1}{2} \frac{\eta}{\eta-1} \left[ -\theta_* + 1 - e^{-\theta_*} \right] \right\}, \end{aligned} \quad (13)$$

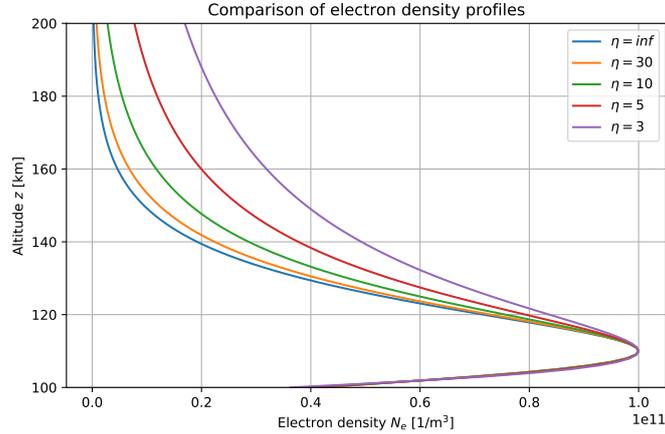
with  $\theta_* = \theta_*(z) = (\eta - 1) \ln \left( 1 + \frac{z-z_*}{\eta H_{n*}^N} \right)$ , and  $H_{n*}^N$  denoting the density scale height at  $z = z_*$ . See Appendix B2 for details. Electron density profiles for identical peak parameters but different values of  $\eta$  are displayed in Figure 2.

125 The electron density model is designed to describe the ionospheric E-layer, assuming that contributions from the F-layer are modeled separately and subtracted from the measurements. To account for residuals that may remain after subtraction, the DIPCont package contains a parameter  $N_{eF}$ .

### 2.5 Ion temperature

In analogy with the neutral temperature case, ion temperature  $T_i$  is assumed to vary linearly with altitude  $z$ :

$$130 \quad T_i(z|z_0, T_{i0}, L_{i0}) = T_{i0} \cdot \left( 1 + \frac{z-z_0}{L_{i0}} \right). \quad (14)$$



**Figure 2.** Altitude dependence of the non-isothermal electron density model for different values of the inverse neutral density scale height gradient  $\eta$ . Common electron density peak parameters are  $z_* = 110$  km,  $N_{e*} = 10^{11} \text{ m}^{-3}$ ,  $H_{n*}^N = 7$  km. The case  $\eta \rightarrow \infty$  (in the legend,  $\eta = \text{inf}$ ) corresponds to the isothermal limit.

The parameters  $T_{i0}$  and  $L_{i0}$  are the ion temperature and the gradient length scale, respectively, at the chosen reference altitude  $z_0$ .

## 2.6 Ion-neutral collision frequency

In quantitative terms, collision processes in the partially ionized LTI medium remain inadequately described, and are major sources of uncertainties in empirical models (e.g., Palmroth et al., 2021; Heelis and Maute, 2020; Sarris, 2019). At this stage, the DIPCont project is less concerned with optimizing the quantitative description of the LTI, but rather with the quality of parameter estimation extrapolation. While the choice of the best LTI model is certainly important for recovering the real values of targeted observables, further work will be needed, by parametric studies, comparison with previous work, and data analysis when a low-perigee mission such as Daedalus (Sarris et al., 2020) provides in situ measurements in the LTI. For our goal here, the chosen variant among the models for ion-neutral collision frequency  $\nu_{in}$  should not matter too much as long as the underlying variability associated with erroneous measurements is captured. To this end, we follow the description of Huba (2019) and write

$$\nu_{in} = \sigma_{in} N_n \sqrt{\frac{kT_i}{m_i}} \quad (15)$$

with the collision cross section  $\sigma_{in} \sim 5 \cdot 10^{-15} \text{ cm}^2$ . An even simpler expression could neglect the variation with ion temperature  $T_i$  so that  $\nu_{in}$  becomes directly proportional to the neutral density  $N_n$ .



Symbol	Description
$z_0$	Local reference altitude
$T_{n0}$	Neutral temperature at $z_0$
$L_{n0}$	Neutral temperature gradient length at $z_0$
$N_{n0}$	Neutral density at $z_0$
$H_{n0}^N$	Neutral density scale height at $z_0$
$\eta = \eta_n$	Inverse gradient of neutral density scale height
$N_{e0}$	Electron density at $z_0$
$L_{r0}$	Radiation absorption length at $z_0$
$\chi$	Inclination angle of incident radiation
$N_{eF}$	F-layer contribution to electron density
$T_{i0}$	Ion temperature at $z_0$
$L_{i0}$	Ion temperature gradient length at $z_0$

**Table 1.** Parameters of model functions in local representation. The list is partially redundant, e.g.,  $L_{n0} = \eta H_{n0}^N$ . The parameters  $L_{r0}$  and  $\chi$  cannot be estimated independently but only in combination  $L_{r0} \cos \chi$ . Boundary data (neutral and ion temperatures at the base of the LTI) are used to constrain the parameters  $L_{n0}$ ,  $\eta$ ,  $H_{n0}^N$ , and  $L_{i0}$ , see Section 3.3.

## 2.7 Pedersen conductivity

Pedersen conductivity is given by

$$\sigma_P = \frac{N_e e^2}{m_i} \frac{\nu_{in}}{\nu_{in}^2 + \Omega_i^2} \quad (16)$$

for a quasi-neutral two-component plasma when the contribution from electron-neutral collisions is neglected, see also Eq. (1), reproduced here for convenience. Compared to other variables and parameters of the LTI models presented here, the ion gyrofrequency  $\Omega_i$  can be determined from measurements or models of the magnetic field with very good accuracy, hence the associated variability should not much affect our results. For simplicity, the ion gyrofrequency is set to a constant.

## 2.8 LTI model in compact form

Parameters of model functions in local representation are listed in Table 1.

The description of the DIPCont modeling procedure in Section 3 benefits from summarizing the LTI model in compact form as  $\mathbf{m} = \mathbf{m}(z|\mathbf{p})$ , with parameters  $T_{n0}, H_{n0}^N, \eta, \dots$ , entering the vector  $\mathbf{p}$ . The parametric functions  $T_n(z), N_n(z), N_e(z), T_i(z), \nu_{in}(z) = \nu_{in}(N_n(z), T_i(z))$ , and  $\sigma_P(z) = \sigma_P(N_e(z), \nu_{in}(z))$  constitute the components of the vectorial function  $\mathbf{m}$ .



### 3 DIPCont modeling procedure

The DIPCont modeling procedure is as follows.

- 160 – Synthetic noise-free measurements  $\mathbf{m}_j = \mathbf{m}(z_j | \mathbf{p})$  are created along anticipated Daedalus satellite orbit sections around perigee at altitudes  $z_j = z(t_j)$  and horizontal distances  $x_j = x(t_j)$ . The chosen model parameters are defined by vectors  $\mathbf{p} = \mathbf{p}(x_{\#})$  on a grid of horizontal distances  $x_{\#}$ . The integration and approximation methods employed for constructing the satellite orbits are described in Section 3.1 and in Appendix C.
- Using the multiplicative noise model presented in Section 3.2, synthetic measurements are contaminated by random  
 165 errors in accordance with relative uncertainties specified in the Daedalus Report for Assessment (ESA, 2020), yielding ensembles  $\{\tilde{\mathbf{m}}_j^k\}$  of noisy synthetic data sets.
- For a point  $x_{\#}$  on the horizontal grid, synthetic data with horizontal distances  $x_j$  in  $[x_{\#} - \Delta x, x_{\#} + \Delta x]$  are considered to produce a least-squares estimate  $\hat{\mathbf{p}}^k(x_{\#})$  of the parameter vector  $\mathbf{p}(x_{\#})$ . Repeating the estimation procedure for all members  $k$  of the ensemble  $\{\tilde{\mathbf{m}}_j^k\}$  of synthetic data sets yields ensembles of model parameters  $\{\hat{\mathbf{p}}^k(x_{\#})\}$  for all  
 170 horizontal grid points  $x_{\#}$ . Specifics of the estimation procedure are discussed in Section 3.3.
- With parameter vectors  $\mathbf{p} \in \{\hat{\mathbf{p}}^k(x_{\#})\}$ , the parametric model function  $\mathbf{m} = \mathbf{m}(z | \mathbf{p})$  can be evaluated to obtain ensembles  $\{\hat{\mathbf{m}}^k(z, x_{\#})\} = \{\mathbf{m}(z | \hat{\mathbf{p}}^k(x_{\#}))\}$ , representing altitude profiles of LTI observables and derived variables such as  $\nu_{in}$  and  $\sigma_p$  over the entire range of LTI altitudes, and for all horizontal grid points  $x_{\#}$ . The resulting altitude profiles form a representative ensemble in the sense that their statistics are compatible with the model functions and the set of given  
 175 relative errors. Relative deviation measures of observables and derived variables as functions of altitude are constructed. Finally, the concept of extrapolation horizons, introduced in Section 3.4, captures the altitude range where errors are tolerable according to predefined thresholds.

#### 3.1 Satellite orbits around perigee

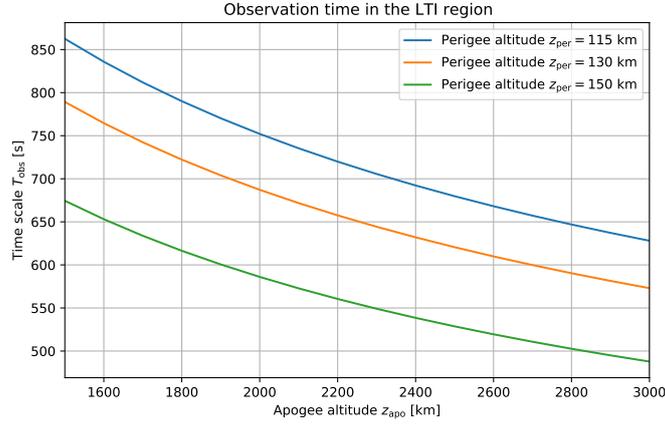
The DIPCont model offers two options for computing altitudes and horizontal distances along the orbits of satellites around  
 180 perigee, namely, numerical integration by means of the Störmer-Verlet method (e.g., Hairer et al., 2003), and the polynomial approximation

$$z(t) = z_{\text{per}} + \frac{a_{\text{per}}}{2} t^2, \quad (17)$$

$$x(t) = \frac{R_{\text{E}} V_{\text{per}} t}{R_{\text{per}}} \left( 1 - \frac{a_{\text{per}}}{3R_{\text{per}}} t^2 \right), \quad (18)$$

with the acceleration  $a_{\text{per}}$  at perigee given by

$$185 \quad a_{\text{per}} = \frac{GM_{\text{E}}}{R_{\text{per}}^2} \frac{R_{\text{apo}} - R_{\text{per}}}{R_{\text{apo}} + R_{\text{per}}} = g_{\text{per}} \varepsilon, \quad (19)$$



**Figure 3.** Observation time  $T_{\text{obs}}$  in the LTI versus apogee altitude  $z_{\text{apo}}$  for three different values of perigee altitude  $z_{\text{per}}$ . The topside of the LTI is assumed to be at  $z_{\text{T}} = 200$  km.

see Appendix C. Here  $R_{\text{E}}$  is the Earth’s radius,  $M_{\text{E}}$  is the Earth’s mass,  $G$  is the gravitational constant,  $z_{\text{per}}$ ,  $R_{\text{per}}$ , and  $V_{\text{per}}$  are the altitude, geocentric distance, satellite velocity at perigee,  $g_{\text{per}} = \frac{GM_{\text{E}}}{R_{\text{per}}^2}$  is the Earth’s gravitational acceleration at geocentric distance  $R_{\text{per}}$ ,  $R_{\text{apo}}$  is the geocentric distance at apogee, and  $\varepsilon = \frac{R_{\text{apo}} - R_{\text{per}}}{R_{\text{apo}} + R_{\text{per}}}$  is the orbital eccentricity. For the parameter range considered in this study, the deviation of the polynomial approximation from the more precise orbit integration is of the order of a few hundred meters.

The observation time  $T_{\text{obs}}$  spent by Daedalus in the LTI during a perigee pass controls the amount of data that can be gathered for statistical investigations. Using the quadratic orbital approximation around perigee,  $T_{\text{obs}}$  is twice the time needed to move from  $z = z_{\text{per}}$  to the upper boundary at  $z = z_{\text{T}}$ , thus  $z_{\text{T}} - z_{\text{per}} = \frac{a_{\text{per}}}{2} (T_{\text{obs}}/2)^2$ ,  $T_{\text{obs}}^2 = \frac{8(z_{\text{T}} - z_{\text{per}})}{a_{\text{per}}}$ , and

$$T_{\text{obs}}^2 = \frac{8(z_{\text{T}} - z_{\text{per}})R_{\text{per}}^2}{GM_{\text{E}}} \frac{R_{\text{apo}} + R_{\text{per}}}{R_{\text{apo}} - R_{\text{per}}} = \frac{8(z_{\text{T}} - z_{\text{per}})}{g_{\text{per}} \varepsilon}. \quad (20)$$

195 The variations of  $T_{\text{obs}}$  with apogee altitude in the range  $1500 \text{ km} \leq z_{\text{apo}} \leq 3000 \text{ km}$  for the three perigee altitudes  $z_{\text{per}} = 115, 130, 150 \text{ km}$  are displayed in Figure 3. Raising the perigee from 115 km to 130 km yields a small reduction of observation time by about 10%. Within the range of orbital parameters considered here, the overall amount of data gathered during a perigee pass turns out to depend only moderately on apogee altitude  $z_{\text{apo}}$ , with a relative difference of not more than about 20% for changes in  $z_{\text{apo}}$  between 2000 km and 3000 km.

### 200 3.2 Synthetic measurements and positivity constraints

Synthetic measurements  $\{\tilde{\mu}_1, \tilde{\mu}_2, \tilde{\mu}_3, \dots\}$  of an observable at altitudes  $\{z_1, z_2, z_3, \dots\}$  are constructed from a parametric model function  $\mu = \mu(z|\mathbf{p})$  producing predictions that are contaminated by random errors  $\{\sigma_1, \sigma_2, \sigma_3, \dots\}$  from a suitable probability distribution. The model parameter vector  $\mathbf{p}$  is estimated through minimization of a cost function. Following the standard least



Observable	Relative error
Neutral temperature $T_n$	0.2
Neutral density $N_n$	0.2
Electron density $N_e$	0.1
Ion temperature $T_i$	0.1

**Table 2.** Relative error levels used in this study, according to Table 2 of the Daedalus Report for Assessment (ESA, 2020).

squares approach, the cost function is chosen to be the error-scaled square deviation

$$205 \quad \chi^2(\mathbf{p}) = \sum_j \left( \frac{\tilde{\mu}_j - \mu(z_j|\mathbf{p})}{\sigma_j} \right)^2. \quad (21)$$

The observables of interest  $T_n$ ,  $N_n$ ,  $N_e$ ,  $T_i$  are all positive, hence a straightforward additive noise model would not be appropriate as it may produce negative synthetic data. Furthermore, instrumental uncertainties as provided in the Daedalus Report for Assessment (ESA, 2020) are typically specified as relative (multiplicative) errors. Both issues are addressed by considering as model predictions  $\mu_j = \mu(z_j|\mathbf{p})$  and data  $\tilde{\mu}_j$  not the positive observables as such but their (natural) logarithms,  
 210 and relative uncertainties for the random errors  $\{\sigma_1, \sigma_2, \sigma_3, \dots\}$ . In the case of a (neutral or electron) density  $N$ , one obtains

$$\ln \tilde{N}_j = \ln N(z_j) + \sigma_j r_j \quad (22)$$

where the  $r_j \sim \mathcal{N}(0, 1)$  represent Gaussian noise (normally distributed random numbers with zero mean and unit variance), and  $N = N(z)$  refers to the (positive) density model. Then

$$\tilde{N}_j = e^{\sigma_j r_j} \cdot N(z_j) \quad (23)$$

215 so that positivity is guaranteed. Furthermore,

$$e^{\sigma_j r_j} \approx 1 + \sigma_j r_j, \quad (24)$$

showing that the parameters  $\sigma_j$  correspond to relative error levels. Table 2 summarizes the values used in this report.

In general, the parameters enter the logarithms of model functions nonlinearly, and an iterative estimation procedure is required.

### 220 3.3 Parameter estimation strategies

The model parameters listed in Table 1 are estimated from observations of neutral temperature  $T_n$ , neutral density  $N_n$ , electron density  $N_e$ , and ion temperature  $T_i$  as follows.

- For a given horizontal grid location  $x_{\#}$ , data within the interval  $[x_{\#} - \Delta x, x_{\#} + \Delta x]$  are considered. The effective window width is  $2\Delta x$ , see the white solid rectangles in Figures 1 and 4.



- 225 – From  $T_n$  data and constraining the neutral temperature profile at the LTI lower boundary  $z_B$  as explained below, infer  $T_{n0}$ ,  $H_{n0}^N$  and  $\eta$ . See Eq. (2) and Section 2.2.
- Using  $H_{n0}^N$  and  $\eta$ , estimate  $N_{n0}$  from  $N_n$  data. See Eq. (11).
- Using  $H_{n0}^N$  and  $\eta$ , estimate  $N_{e0}$  and  $L_{r0} \cos \chi$  from  $N_e$  data. See Eq. (12).
- From  $T_i$  data and a suitable constraint at the LTI lower boundary  $z_B$  in analogy to the neutral temperature case, infer  $T_{i0}$   
 230 and  $L_{i0}$ . See Eq. (14).

Altitude profiles of these observables allow for constructing the height dependence of derived variables such as ion-neutral collision frequency  $\nu_{in}$  and the Pedersen conductivity  $\sigma_P$ , see Eqs. (15) and (16), respectively.

### Lower LTI boundary constraints

As explained in Appendix A, Eqs. (A10) and (A13), the linear density scale height profile can be parametrized using  $H_{n0}^N$  and  
 235  $\eta$  in the form

$$H_n^N(z|z_0, H_{n0}^N, \eta) = H_{n0}^N \cdot \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right). \quad (25)$$

It is important to note that the  $H_n^N$  profile takes center stage in the LTI models of the observables  $T_n$ ,  $N_n$ , and  $N_e$ . While the local temperature amplitude  $T_{n0}$  is essentially an average of local temperature data around an altitude  $z_0$ , and the same applies to the local pressure scale height  $H_{n0}^P$  obtained from  $T_{n0}$  by simple multiplication, the inverse density scale height gradient  $\eta$   
 240 and thus also the local density scale height parameter  $H_{n0}^N = \frac{\eta-1}{\eta} H_{n0}^P$  are very challenging to estimate from purely local data with little variance in altitude, as suggested already by the standard error of the slope in linear regression analysis. Fortunately, neutral temperature at the base of the LTI is known with reasonable tolerances from atmospheric models (e.g., Picone et al., 2002). This remote data point constitutes a valuable constraint for estimating the density scale height profile. To incorporate model uncertainties and expected deviations from actual values, boundary data at the base of the LTI are contaminated by  
 245 random errors according to the approach described in Section 3.2.

To be specific, the pressure scale height gradient as given in Eq. (5), constant under the assumptions discussed in Section 2.2 and Appendix A, can be obtained from its values  $H_{n0}^P$  and  $H_{nB}^P$  at  $z_0$  and the LTI base altitude  $z_B$ , respectively, as follows:

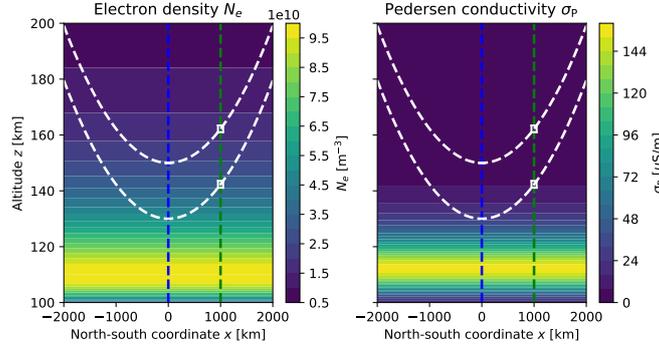
$$\frac{dH_n^P}{dz} = \frac{H_{n0}^P - H_{nB}^P}{z_0 - z_B}. \quad (26)$$

The inverse gradients  $\gamma$  and  $\eta$  of pressure scale height and density scale height, respectively, are related by Eq. (8) through  
 250  $\eta = \gamma + 1$ , thus the parameter  $\eta$  is given by

$$\eta = \frac{z_0 - z_B}{H_{n0}^P - H_{nB}^P} + 1 = \frac{M_n g}{R_{\text{gas}}} \frac{z_0 - z_B}{T_{n0} - T_{nB}} + 1, \quad (27)$$

where  $T_{nB}$  denotes the neutral temperature at  $z_B$ . The local density scale height  $H_{n0}^N$  can now be obtained from Eq. (9) as

$$H_{n0}^N = \frac{H_{n0}^P}{1 + \gamma^{-1}} = \frac{\eta - 1}{\eta} \frac{R_{\text{gas}} T_{n0}}{M_n g}. \quad (28)$$



**Figure 4.** Model distributions of electron density  $N_e$  (left panel) and Pedersen conductivity  $\sigma_P$  (right panel) in the LTI. Synthetic measurements are produced along the two satellite orbits (white dashed lines). The parameters of vertical profiles are estimated using measurements within a window (white solid rectangle) around two locations in horizontal direction (blue and green dashed lines).

### Linear estimation of electron density parameters

255 The logarithm of the electron density model considered here,

$$\ln N_e(z) = \ln N_{e0} + \frac{1}{2} \frac{\eta}{\eta - 1} \left[ -\theta_0 + \frac{H_{n0}^N}{L_{r0} \cos \chi} (1 - e^{-\theta_0}) \right], \quad (29)$$

can be combined with the logarithm of the neutral density model,

$$\ln N_n(z) = \ln N_{n0} - \frac{\eta}{\eta - 1} \theta_0, \quad (30)$$

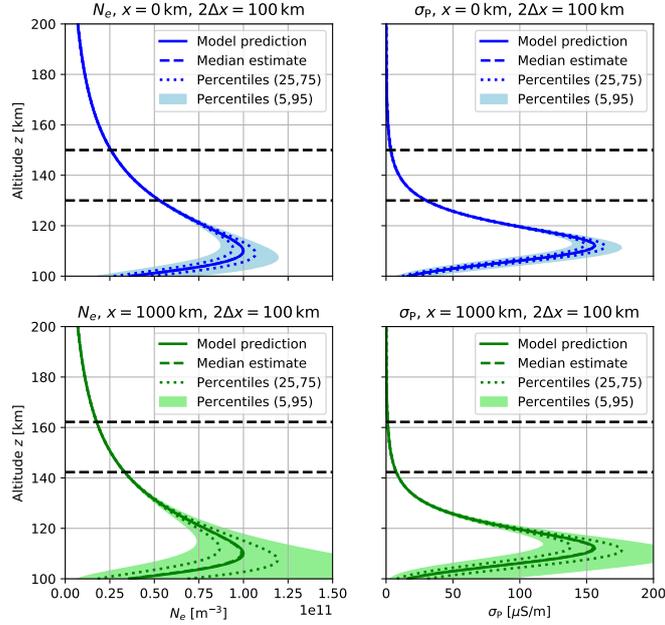
to find

$$\begin{aligned} & \ln N_e(z) - \frac{1}{2} \ln N_n(z) \\ 260 \quad & = \ln N_{e0} - \frac{1}{2} \ln N_{n0} + \frac{1}{2} \frac{\eta}{\eta - 1} \frac{H_{n0}^N}{L_{r0} \cos \chi} (1 - e^{-\theta_0}) \\ & = a + b(1 - e^{-\theta_0}), \end{aligned} \quad (31)$$

showing that  $a = \ln N_{e0} - \frac{1}{2} \ln N_{n0}$  and  $b = \frac{1}{2} \frac{\eta}{\eta - 1} \frac{H_{n0}^N}{L_{r0} \cos \chi}$  can be obtained from linear regression of  $\ln N_e - \frac{1}{2} \ln N_n$  versus  $1 - e^{-\theta_0}$  with  $\theta_0 = \theta_0(z) = (\eta - 1) \ln \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right)$ . Since the parameters  $\eta$  and  $H_{n0}^N$  are available as estimates from  $T_n$  modeling, and  $N_{n0}$  is known from  $N_n$  modeling,  $N_{e0}$  and  $L_{r0} \cos \chi$  can be computed from the linear coefficients  $a$  and  $b$ , hence this special case does not necessitate an iterative parameter estimation approach.

### 265 3.4 Error profiles and extrapolation horizons

With  $\{\tilde{\mathbf{m}}_j^k\}_{j \in [\#]}^{k=1}$  being a single set ( $k = 1$ ) of synthetic measurements, and  $j \in [\#]$  indicating that horizontal distances are selected to be within  $\pm \Delta x$  around a predefined grid point  $x_\#$ , the estimation procedure yields a specific estimate  $\hat{\mathbf{p}}^k$  of



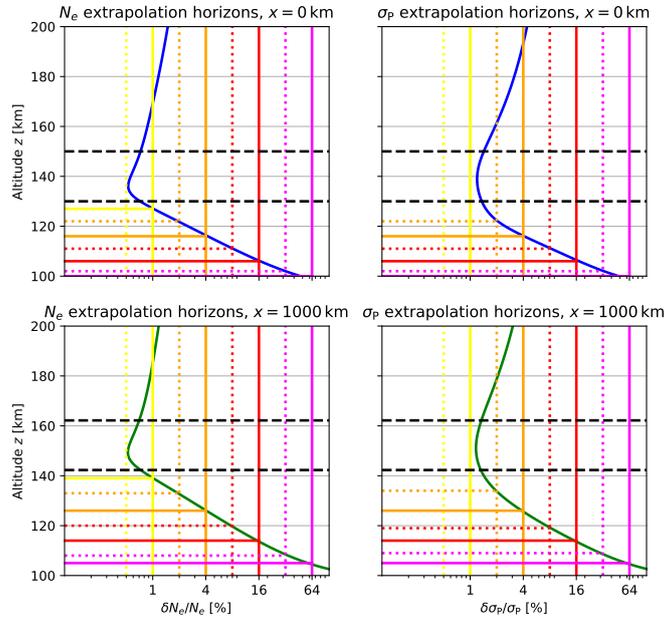
**Figure 5.** Visualization of the ensemble of altitude profiles generated from the Monte Carlo distributions of model parameters. Shown are selected quantiles evaluated at the vertical grid of LTI altitudes. Left panels: electron density  $N_e$ . Right panels: Pedersen conductivity  $\sigma_p$ . Upper panels: center position (blue dashed line) in Figure 4. Lower panels: right position (green dashed line) in Figure 4.

the parameter vector  $\mathbf{p}(x_{\#})$ . In a Monte Carlo setup, different instances of random errors are applied to the model predictions to produce data sets  $\{\tilde{\mathbf{m}}_j^1, \tilde{\mathbf{m}}_j^2, \tilde{\mathbf{m}}_j^3, \dots\}_{j \in \{\#\}}$ . The ensemble of data sets gives rise to an ensemble of parameter vectors  $\{\hat{\mathbf{p}}^k\} = \{\hat{\mathbf{p}}^1, \hat{\mathbf{p}}^2, \hat{\mathbf{p}}^3, \dots\}$ , which in turn, when entered in  $\mathbf{m} = \mathbf{m}(z|\mathbf{p})$ , yields an ensemble of profiles  $\{\hat{\mathbf{m}}^k(z, x_{\#})\} = \{\hat{\mathbf{m}}^1(z, x_{\#}), \hat{\mathbf{m}}^2(z, x_{\#}), \hat{\mathbf{m}}^3(z, x_{\#}), \dots\}$  for the entire range of altitudes  $z$ , and at each point  $x_{\#}$  of the horizontal coordinate grid.

The procedure is illustrated in Figures 4 and 5. Figure 4 shows the model functions and the satellite orbits used for computing the predictions that enter the Monte Carlo simulation. The ensemble of altitude profiles generated from the Monte Carlo distributions of model parameters is visualized in Figure 5 by means of selected quantiles evaluated at the vertical grid of LTI altitudes.

The ensemble of altitude profiles forms the basis for quantifying extrapolation quality through measures of relative deviation from a model prediction. Suppressing altitude and horizontal grid dependencies, and considering only a single model variable  $\mu$  with ensemble members  $\hat{\mu}^1, \hat{\mu}^2, \hat{\mu}^3, \dots, \hat{\mu}^K$ , the root-mean-square deviation is given by

$$\delta\mu = \sqrt{\langle (\hat{\mu} - \mu)^2 \rangle} = \sqrt{\frac{1}{K} \sum_{k=1}^K (\hat{\mu}^k - \mu)^2}. \quad (32)$$



**Figure 6.** Solid lines (blue and green) give the relative root-mean-square deviations of Monte Carlo altitude profiles from the respective input model profiles at two horizontal locations. Vertical dotted and solid lines represent a set of chosen error levels, ranging from 0.5 % and 1 % (yellow) to 32% and 64% (magenta). The corresponding horizontal lines show the extrapolation horizons indicating at which altitude the relative deviation equals the respective error level. Left panels: electron density  $N_e$ . Right panels: Pedersen conductivity  $\sigma_p$ . Upper panels: center position (blue dashed line) in Figure 4. Lower panels: right position (green dashed line) in Figure 4.

Figure 6 shows the altitude profiles of *relative* root-mean-square deviation  $\delta\mu/\mu = \sqrt{\langle(\hat{\mu} - \mu)^2\rangle}/\mu$  for the variables and horizontal locations as in Figures 4 and 5.

Alternative relative deviation measures considered in the DIPCont package are based on the empirical distribution of absolute deviations  $|\hat{\mu} - \mu|$ , e.g., the average absolute deviation from the model prediction  $\mu$ :

$$285 \quad (\delta\mu)_{\text{abs}} = \langle|\hat{\mu} - \mu|\rangle = \frac{1}{K} \sum_{k=1}^K |\hat{\mu}^k - \mu|, \quad (33)$$

or selected quantiles of the distribution.

### 3.5 Implementation

The DIPCont model is implemented as a bundle of Python instructions and functions collected in three modules.

In the module `DIPContBas.py`, the basic setup of the DIPCont framework is defined, e.g., LTI region boundaries and  
 290 boundary values, satellite orbit parameters, horizontal grid locations, and auxiliary plot parameters. Furthermore, it also pro-



vides configurational variables that are exchanged between DIPCont functions and modules, e.g., parameters shared by different parametric models.

The module `DIPContMod.py` provides parametric model functions of LTI variables and plot routines.

295 The module `DIPContEst.py` is concerned with Monte Carlo parameter estimation and profile continuation. Estimation of parameters that enter the model functions nonlinearly is accomplished by the function `curve_fit()` from the module `scipy.optimize` whereas linear parameter estimation is performed using the function `linregress` from the module `scipy.stats`. Monte Carlo ensembles of parameters and altitude profiles are stored in `pandas` dataframes.

The three DIPCont modules are provided as supplementary files to this report, together with Jupyter notebooks to explain and illustrate their usage.

## 300 4 First results

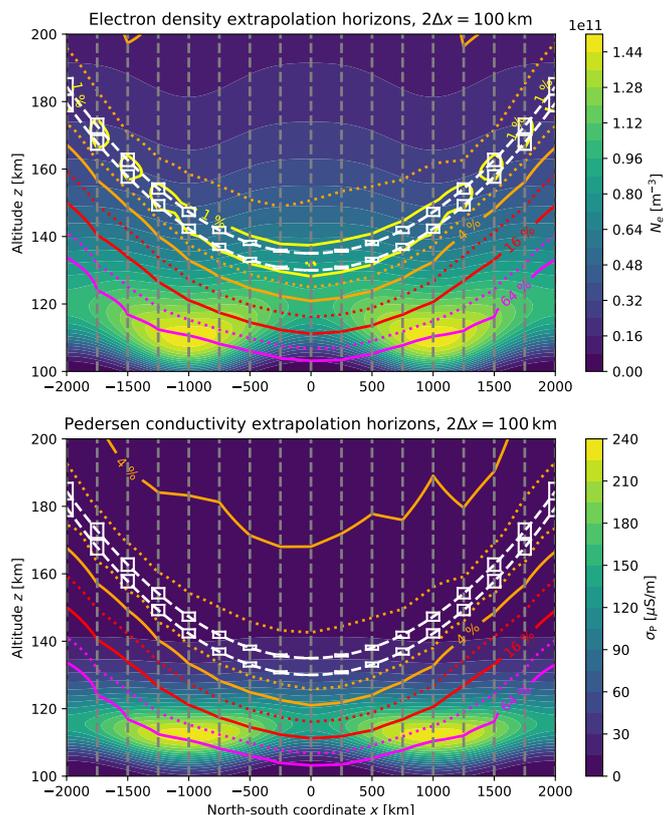
The major ingredients of the DIPCont processing chain, namely, generation of synthetic in-situ measurements along satellite orbits, Monte Carlo simulations of vertical profiles, and construction of extrapolation horizons, are summarized in Figures 4–6 displaying electron density  $N_e$  and Pedersen conductivity  $\sigma_P$  as two variables of key importance for the structure and the dynamics of the LTI. As indicated by Eq. (1) and the respective profiles in Figure 5, electron density makes the main contribution 305 to the peaked height variation of Pedersen conductivity, with secondary contributions of neutral density and possibly ion temperature through the parametric form chosen for the ion-neutral collision frequency, see Section 2.6. Furthermore, Pedersen conductivity controls the height variation of Joule heating, whose characterization is one of the main scientific targets of the proposed Daedalus mission (ESA, 2020).

When instead of two selected horizontal locations as in Figure 6 an equidistant grid of horizontal coordinates is defined for 310 DIPCont simulations and the construction of extrapolations horizons, the results can be displayed together with the underlying model distributions and satellite orbits as in Figure 1. In the following examples, such displays are used to visualize DIPCont results for different spacecraft configurations. Section 4.1 offers a first qualitative assessment of extrapolation quality in terms of varying inter-spacecraft distance. Section 4.2 contrasts the performance of the dual-spacecraft configuration considered so far with the results of the single-spacecraft case.

315 Note that the horizontal axis corresponds to the latitudinal (north-south) direction. In the simulations that led to Figures 4–6, horizontal variations were disregarded for better comparability. In Figure 1 and in the following, latitudinal inhomogeneity of electron density is meant to reproduce the two maxima observed by a polar orbiting satellite when crossing the auroral oval. The highest latitude corresponds to the origin of the horizontal axis.

### 4.1 Varying inter-spacecraft distance

320 Extrapolation of two-point measurements is expected to perform best if the spatial separation matches the relevant physical length scale. In the LTI this should be the (local) density scale height, in the range of 10–20 km for altitudes above 130 km, as in our example of a dual-spacecraft setup with perigee altitudes of 130 km and 150 km, see Figure 1. The inter-spacecraft



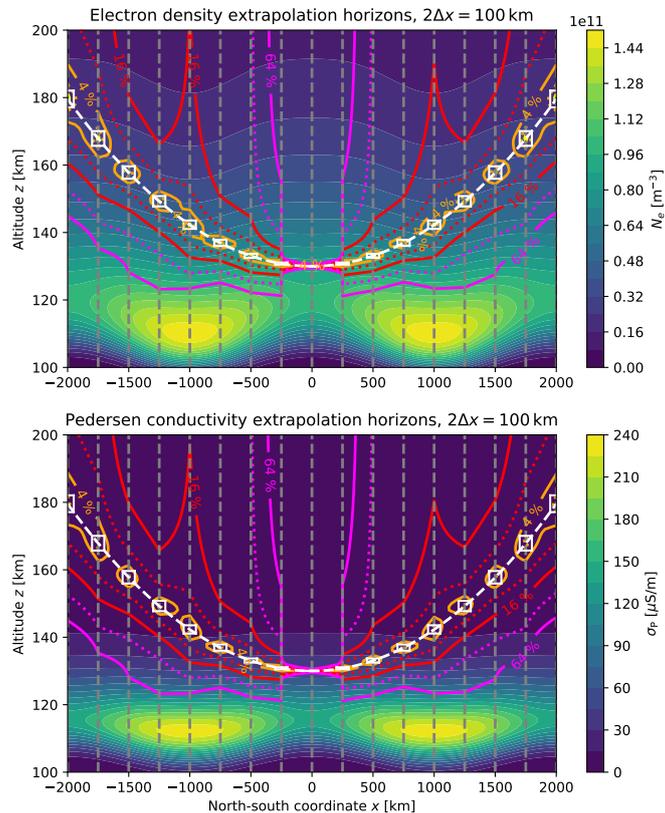
**Figure 7.** Same as Figure 1 but for an inter-spacecraft separation of 5 km at perigee.

distance remains close to 20 km throughout the whole orbit section and thus also to the density scale height as the relevant physical scale.

325 Figure 7 displays extrapolation horizons for the same simulation setup except that the perigee altitude of the second satellite is reduced to 135 km, producing an inter-spacecraft distance at perigee of only 5 km. The separation is now smaller than the local density scale height with values of about 15 km at altitudes around 150 km. Compared to Figure 1, the errors are increased and the extrapolation horizons reduced. The changes are not dramatic but enough to show that inter-spacecraft distance is a parameter to be considered when extrapolation quality is supposed to be optimized.

#### 330 4.2 Single-satellite case

To check how much a second satellite improves extrapolation quality, the Monte Carlo simulations summarized in Figure 1 are repeated for the single-spacecraft case, with all other parameters left unchanged. The resulting extrapolation horizons are shown in Figure 8. Compared to ionospheric profile continuation from dual-spacecraft observations, the single-spacecraft case yields significantly worse results, with extrapolation horizons collapsing into the orbit near the perigee due to lacking variability



**Figure 8.** Same as Figure 1 but for the single-satellite case.

335 in altitudes. Away from the perigee, the orbital motion of the satellite during the time corresponding to the horizontal window width  $2\Delta x$  yields some height range that allows for profile reconstruction but with significant errors. The peaks in electron density and Pedersen conductivity are clearly outside the largest considered error level of 64%, while Figure 1 shows that in the dual-spacecraft case the peaks are between the 16% and 32% error levels.

## 5 Discussion

340 Our first results suggest that altitude profiles of key LTI variables can be reconstructed with sufficient accuracy from in-situ measurements if the effective altitude range covers relevant physical scales such as the local density scale height  $H_{r0}^N$ . This is the case for a dual-spacecraft configuration with an inter-spacecraft separation of 20 km at perigee, see Figures 1 and 4–6. By two-point sampling, one can retrieve the vertical profiles of electron density and Pedersen conductivity essentially down to the bottom of the LTI region, a few scale heights under the lower satellite and including the peak altitudes. For Pedersen



345 conductivity, errors are expected in the range of several 10%, with the peak altitude and most of the conductivity within the 32% extrapolation horizon in the chosen example, consistent with rocket observations (Sangalli et al., 2009).

Given the current knowledge of key LTI variables, error levels of a few ten percent may well improve the situation. An important motivation behind the Daedalus proposal was the large error margin in Joule heating estimates, with a major contribution by errors in conductance (height-integrated conductivity). Thus, Sarris et al. (2020) pointed out that for a substorm event investigated by Palmroth et al. (2005), there were differences of up to 500% between three proxies of the Joule heating rates integrated over the Northern hemisphere. Even if this setup cannot be directly compared to our virtual environment, the order of magnitude difference between the two error margins looks encouraging for follow-up work on ionospheric profile continuation.

The DIPCont framework allows for addressing economical and technical questions regarding the impact of different LTI mission cost factors. On the one hand, a dual-spacecraft mission seems to automatically imply higher costs because a second satellite needs to be built. On the other hand, a major cost driver of any deep LTI mission is the necessary amount of propellant that is required in order to maintain a spacecraft in orbit, due to enhanced atmospheric drag at very low perigee altitudes. Since in a dual spacecraft setup the role of the lower perigee satellite can be shared, each of the two probes would have to carry half of the total amount of propellant required to maintain the same total observation time required by a single-satellite mission. Moreover, the necessary amount of thermal shielding depends as well on perigee altitude and each of the two probes would have to withstand the maximum thermal stress at perigee less often. Our findings show that the two-point setup allows for a more effective extrapolation to lower altitudes, which in turn means that a higher perigee may well be a meaningful option.

Data processing would also benefit from raising the perigee. As shown by simulations carried out for the technical assessment of Daedalus (ESA, 2020), a hydrodynamic shock develops in front of the spacecraft at altitudes under  $\sim 120\text{--}130$  km, complicating the retrieval of unperturbed data from the observed ones. Another LTI mission parameter considered in this paper is the apogee altitude controlling the proximity to the Van Allen belts and thus the necessary amount of radiation shielding, but affecting also the the available LTI observation time near perigee. The analysis presented in Section 3.1 shows that the amount of data gathered for statistical studies depends only moderately on apogee altitude.

The current version of the DIPCont framework concentrates on the E-layer, assuming that contributions from the F-layer can be disregarded or subtracted before processing, e.g., using the NeQuick approach to model topside ionospheric sounding data (Pignalberi et al., 2020). The DIPCont package contains a parameter  $N_{eF}$  to study the effect of F-layer residuals on extrapolation quality in future work.

The first results presented here are planned to be validated and extended in more extensive studies. Besides varying orbital parameters such as perigee altitude and inter-spacecraft distance, the impact of numerical parameters such as the horizontal selection window,  $2\Delta x$ , needs further investigation. As already commented in Section 2.6, alternative functional forms for modeling ion-neutral collision frequencies or other variables may also be considered.



## 6 Conclusions and Outlook

The DIPCont framework enables a systematic approach to reconstructing ionospheric vertical profiles and quantitatively assessing extrapolation quality. DIPCont allows for linear temperature variation with altitude, which extends the often used isothermal model and provides a solid foundation to future applications, based on more complex models and on real world data. By quantifying the quality of extrapolated in-situ measurements, DIPCont can help to assess the science return of specific configurations and thus to optimize the parameters of upcoming LTI missions.

First DIPCont tests, performed on electron density and Pedersen conductivity, show promising results, to be consolidated by further parametric studies. Application of DIPCont to a modeled event, like the geomagnetic storm event of March 2015 addressed in the Daedalus Report for Assessment (ESA, 2020) is an upcoming target. Future studies are planned to include Joule heating which was a major driver of the Daedalus mission proposal.

Coordination between an LTI mission, like Daedalus, and a topside mission, e.g., like Swarm or DMSP, would enhance the return of both missions. As an example, reconstruction of vertical profiles of ionospheric conductivity based on LTI observations could help to calibrate topside estimates of the conductance, while topside electron density could provide upper continuation and constrain the height-integrated total electron content (TEC) inferred from LTI data. Combination with ground-based observatory data such as ionosondes would offer further valuable constraints to DIPCont, and thus enable more comprehensive modeling of the LTI.

*Code availability.* The DIPCont framework is implemented in three Python modules `DIPContBas.py`, `DIPContMod.py`, and `DIPContEst.py`. The modules are provided as supplementary files to this report, together with Jupyter notebooks to explain and illustrate their usage. The DIPCont code is planned to be migrated to a public repository.

## Appendix A: Neutral density profile for linear variations of scale height

Consider an atmospheric layer dominated by possibly several neutral constituents with an average or representative particle mass  $m_n$ , total pressure  $P_n$ , mass density  $\rho_n$ , effective neutral number density  $N_n = \rho_n/m_n$  and temperature  $T_n$ . Under hydrostatic conditions,  $dP_n = -\rho_n g dz$ , where  $z$  is altitude and  $g$  is gravity (gravitational acceleration) assumed to vary so little within the layer that it can be safely considered constant. Using the ideal gas law  $P_n = N_n k T_n$  where  $k$  denotes the Boltzmann constant, one obtains  $dP_n = -P_n \frac{m_n g}{k T_n} dz = -P_n \frac{dz}{H_n^P}$  with the pressure scale height

$$H_n^P = \frac{k T_n}{m_n g}, \quad (\text{A1})$$

Rearranging  $-\frac{dz}{H_n^P} = \frac{dP_n}{P_n} = d \ln P_n$  and integrating leads to

$$P_n(z) = P_{n0} \exp \left\{ - \int_{z_0}^z \frac{d\tilde{z}}{H_n^P(\tilde{z})} \right\} \quad (\text{A2})$$



405 where the altitude dependence of  $H_n^P$  directly reflects the change of temperature  $T_n$  with  $z$ .

Combining the differential of the ideal gas law  $dP_n = N_n k dT_n + k T_n dN_n$  with the hydrostatic condition yields  $-N_n m_n g dz = N_n k dT_n + k T_n dN_n$  and thus  $-\frac{m_n g}{k T_n} dz - \frac{1}{T_n} dT_n = \frac{1}{N_n} dN_n = d \ln N_n$ . Since  $\frac{dT_n}{T_n} = d \ln T_n = d \ln H^P = \frac{dH_n^P}{H_n^P}$ , one obtains

$$\frac{d \ln N_n}{dz} = -\frac{1}{H_n^P} \left( 1 + \frac{dH_n^P}{dz} \right). \quad (\text{A3})$$

410 Introducing the density scale height

$$H_n^N = H_n^P \left( 1 + \frac{dH_n^P}{dz} \right)^{-1}, \quad (\text{A4})$$

the resulting differential equation  $d \ln N_n = -\frac{dz}{H_n^N}$  is integrated to yield

$$N_n(z) = N_{n0} \exp \left\{ -\int_{z_0}^z \frac{d\tilde{z}}{H_n^N(\tilde{z})} \right\}. \quad (\text{A5})$$

To be more specific, we suppose the neutral temperature  $T_n$  varies linearly with altitude  $z$ ,

$$415 \quad T_n(z) = T_{n0} \cdot \left( 1 + \frac{z - z_0}{L_{n0}} \right). \quad (\text{A6})$$

where  $T_{n0}$  is the temperature at a reference altitude  $z_0$ , and  $L_{n0} = \frac{T_{n0}}{dT_n/dz}$  denotes the local gradient length. Then

$$H_n^P(z) = H_{n0}^P \cdot \left( 1 + \frac{z - z_0}{L_{n0}} \right). \quad (\text{A7})$$

with

$$H_{n0}^P = \frac{k T_{n0}}{mg}, \quad (\text{A8})$$

420 so that the pressure scale height gradient  $\frac{dH_n^P}{dz} = \frac{H_{n0}^P}{L_{n0}}$  is constant, and thus also the gradient of density scale height:

$$\frac{dH_n^N}{dz} = \frac{dH_n^P}{dz} \cdot \left( 1 + \frac{dH_n^P}{dz} \right)^{-1}. \quad (\text{A9})$$

The linear profile of density scale height is given by

$$H_n^N(z) = H_{n0}^N \cdot \left( 1 + \frac{z - z_0}{L_{n0}} \right), \quad (\text{A10})$$

with

$$425 \quad H_{n0}^N = \frac{H_{n0}^P}{1 + H_{n0}^P/L_{n0}} = \frac{H_{n0}^P}{1 + \gamma^{-1}}. \quad (\text{A11})$$

Here

$$\gamma = \left( \frac{dH_n^P}{dz} \right)^{-1} \quad (\text{A12})$$



denotes the inverse gradient of pressure scale height. The inverse gradient of density scale height

$$\eta = \left( \frac{dH_n^N}{dz} \right)^{-1} = \frac{L_{n0}}{H_{n0}^N} \quad (\text{A13})$$

430 is related to  $\gamma$  through  $\eta = \gamma + 1$ .

In the non-isothermal case  $L_{n0} < \infty$ , integrating  $1/H_n^N$  gives the expression

$$\begin{aligned} \zeta_0 &= \int_{z_0}^z \frac{d\tilde{z}}{H_n^N(\tilde{z})} = \eta \ln \left( 1 + \frac{z - z_0}{L_{n0}} \right) \\ &= -\ln \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right)^{-\eta}, \end{aligned} \quad (\text{A14})$$

Hence, the altitude profile of number density (A5) is given by

$$435 \quad N_n(z) = N_{n0} \cdot e^{-\zeta_0} = N_{n0} \cdot \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right)^{-\eta}. \quad (\text{A15})$$

In the isothermal limit,  $\eta \rightarrow \infty$ ,  $\ln \left( 1 + \frac{z - z_0}{\eta H_{n0}^N} \right) \rightarrow \frac{z - z_0}{\eta H_{n0}^N}$ , thus  $\zeta_0 \rightarrow \frac{z - z_0}{H_{n0}^N}$ , and  $H_{n0}^N \rightarrow H_{n0}^P$  through Eq. (A11).

## Appendix B: Electron density profile for linear variations of scale height

Following the approach first presented by Chapman (1931), the ionization rate per unit volume  $q$  is expressed in terms of the intensity  $I$  of ionizing radiation, the ionization efficiency  $\kappa$ , the angle  $\chi$  of incident radiation with the atmospheric layer normal vector, the radiation absorption cross-section  $\sigma_r$ , and the neutral density  $N_n$  as  $q = \kappa \cos \chi \frac{dI}{dz}$ . The function  $q = q(z)$  is also called production function. Although originally proposed for photoionization, the Chapman approach may be applied also to ionization by precipitation of energetic particles as in the auroral region, if model variables and coefficients are properly interpreted.

The intensity  $I$  satisfies the differential equation

$$445 \quad dI = \sigma_r N_n I \frac{dz}{\cos \chi} \quad (\text{B1})$$

with the solution

$$I(z) = I_\infty \exp \left\{ \frac{\sigma_r}{\cos \chi} \int_{z_\infty}^z N(\tilde{z}) d\tilde{z} \right\} \quad (\text{B2})$$

where  $z_\infty$  and  $I_\infty$  refer to an upper boundary sufficiently remote from the atmospheric layer.

Using  $dI = \sigma_r N_n I \frac{dz}{\cos \chi}$ , the production function  $q$  can be rewritten as  $q = \kappa \sigma_r N_n I$  and thus

$$450 \quad q(z) = \kappa \sigma_r N_n(z) I_\infty \exp \left\{ \frac{\sigma_r}{\cos \chi} \int_{z_\infty}^z N(\tilde{z}) d\tilde{z} \right\}. \quad (\text{B3})$$



The ionization peak altitude  $z_*$  is obtained from the condition

$$0 = \left. \frac{d \ln q}{dz} \right|_{z=z_*} = \frac{N'_n(z_*)}{N_n(z_*)} + \frac{\sigma_r N_n(z_*)}{\cos \chi} \quad (\text{B4})$$

where the prime denotes differentiation with respect to altitude  $z$ . Considering Eqs. (A5) and (A14) gives rise to  $N_n(z) = N_{n0} e^{-\zeta_0}$ ,  $\zeta'_0 = 1/H_n^N$ , and defining the *radiation absorption length*  $L_r = L_r(z)$  by

$$455 \quad L_r = \frac{1}{\sigma_r N_n}, \quad (\text{B5})$$

the general ionization peak condition is conveniently expressed as

$$H_n^N(z_*) = L_r(z_*) \cos \chi. \quad (\text{B6})$$

### B1 Local representation of electron density

Assuming the neutral temperature  $T_n$  varies linearly with altitude  $z$ , the altitude dependence of electron density was modeled  
 460 by Gledhill and Szendrei (1950). Since their formulation does not fit well with the DIPCont nomenclature used in the current report, an independent and extended derivation is presented now. Using  $T_n(z) = T_{n0} \cdot \left(1 + \frac{z-z_0}{L_{n0}}\right) = T_{n0} \cdot \left(1 + \frac{z-z_0}{\eta H_{n0}^N}\right)$ , and  $\eta < \infty$ , the altitude profile of neutral number density can be written in the form

$$N_n(z) = N_{n0} \left(1 + \frac{z-z_0}{\eta H_{n0}^N}\right)^{-\eta}, \quad (\text{B7})$$

see Appendix A and Eq. (A15). Integration gives

$$465 \quad \int_{z_\infty}^z N_n(\tilde{z}) d\tilde{z} = -N_{n0} \frac{\eta H_{n0}^N}{\eta - 1} \left[ \left(1 + \frac{\tilde{z}-z_0}{\eta H_{n0}^N}\right)^{-(\eta-1)} \right]_{\tilde{z}=z_\infty}^{\tilde{z}=z}. \quad (\text{B8})$$

In this LTI modeling context it is safe to assume that the regional temperature increase with altitude is moderate enough to ensure  $H_{n0}^N < L_{n0}$ , then  $\eta > 1$ . Furthermore, the altitude  $z_\infty$  is chosen to be large enough for the contribution from the value at  $\tilde{z} = z_\infty$  to be negligible. We obtain

$$\int_{z_\infty}^z N_n(\tilde{z}) d\tilde{z} = -N_{n0} \frac{\eta H_{n0}^N}{\eta - 1} \left(1 + \frac{z-z_0}{\eta H_{n0}^N}\right)^{-(\eta-1)} \quad (\text{B9})$$

470 by using Eq. (A14). Defining

$$\theta_0 = \frac{\eta - 1}{\eta} \zeta_0 = (\eta - 1) \ln \left(1 + \frac{z-z_0}{\eta H_{n0}^N}\right), \quad (\text{B10})$$

the radiation intensity profile assumes the form

$$I(z) = I_\infty \exp \left\{ -\frac{\sigma_r N_{n0}}{\cos \chi} \frac{\eta H_{n0}^N}{\eta - 1} e^{-\theta_0} \right\} \quad (\text{B11})$$

$$= I_\infty \exp \left\{ -\frac{\eta}{\eta - 1} \frac{H_{n0}^N}{L_{r0} \cos \chi} e^{-\theta_0} \right\} \quad (\text{B12})$$



475 where  $L_{r0} = L_r(z_0)$ . The neutral density (A15) is rewritten as

$$N_n(z) = N_{n0} \exp \left\{ -\frac{\eta}{\eta-1} \theta_0 \right\}, \quad (\text{B13})$$

so that the production function (B3) assumes the form

$$q(z) = \frac{\kappa I_\infty}{L_{r0}} \exp \left\{ \frac{\eta}{\eta-1} \left[ -\theta_0 - \frac{H_{n0}^N}{L_{r0} \cos \chi} e^{-\theta_0} \right] \right\}. \quad (\text{B14})$$

480 In the isothermal limit,  $\eta \rightarrow \infty$ ,  $\frac{\eta}{\eta-1} \rightarrow 1$ ,  $\theta_0 \rightarrow \frac{z-z_0}{H_{n0}^N}$ , and the isothermal Chapman production function (Chapman, 1931) is recovered.

In static equilibrium of photoionization and quadratic recombination,  $q = \alpha N_e^2$  with the recombination coefficient  $\alpha$ , thus  $N_e = \sqrt{q/\alpha}$ . Using

$$N_{e0} = N_e(z_0) = \sqrt{\frac{\kappa I_\infty}{\alpha L_{r0}}} \exp \left\{ -\frac{1}{2} \frac{\eta}{\eta-1} \frac{H_{n0}^N}{L_{r0} \cos \chi} \right\}, \quad (\text{B15})$$

we obtain

$$485 N_e(z) = N_{e0} \exp \left\{ \frac{1}{2} \frac{\eta}{\eta-1} \left[ -\theta_0 + \frac{H_{n0}^N}{L_{r0} \cos \chi} (1 - e^{-\theta_0}) \right] \right\}. \quad (\text{B16})$$

## B2 Representation of electron density in terms of ionization peak parameters

A meaningful regional representation of the electron density can be constructed by means of the ionization peak parameters. For a given incident radiation angle  $\chi$ , the altitude  $z_*$  of the electron density maximum can be expressed in local parameters as follows:

$$490 z_* = z_0 + \eta H_{n0}^N \left[ \Gamma^{1/(\eta-1)} - 1 \right]. \quad (\text{B17})$$

where

$$\Gamma = \frac{H_{n0}^N}{L_{r0} \cos \chi}. \quad (\text{B18})$$

The electron density peak value  $N_{e*} = N_e(z = z_*)$  is

$$N_{e*} = N_{e0} \exp \left\{ \frac{1}{2} \frac{\eta}{\eta-1} [-\ln \Gamma + \Gamma - 1] \right\}. \quad (\text{B19})$$

495 With  $z_*$  as the reference altitude,  $z_0 = z_*$ , we can take advantage of the condition (B6)  $H_{n0}^N = H_{n*}^N = L_{r*} \cos \chi = L_{r0} \cos \chi$ , thus

$$N_e(z) = N_{e*} \exp \left\{ \frac{1}{2} \frac{\eta}{\eta-1} [-\theta_* + 1 - e^{-\theta_*}] \right\}, \quad (\text{B20})$$

where  $\theta_* = \theta_*(z) = (\eta-1) \ln \left( 1 + \frac{z-z_*}{\eta H_{n*}^N} \right)$ , and  $H_{n*}^N$  denotes the density scale height at  $z = z_*$ . This representation shows that  $\chi$  is only an implicit parameter of the electron density model, and cannot be inferred from knowledge of the peak parameters.



## 500 Appendix C: Orbit approximation around perigee

Consider a Kepler orbit with radial distance  $r = r(t)$  and azimuth  $\phi = \phi(t)$  where  $t$  denotes time. Distance and velocity at perigee are  $R_{\text{per}}$  and  $V_{\text{per}}$ , respectively. The corresponding variables at apogee are  $R_{\text{apo}}$  and  $V_{\text{apo}}$ , the gravitational constant is  $G$ , and the planetary mass is  $M$ . Combining the conservation laws for angular momentum

$$r^2 \dot{\phi} = R_{\text{apo}} V_{\text{apo}} = R_{\text{per}} V_{\text{per}} \quad (\text{C1})$$

505 and total energy  $E$  (here normalized by the test mass  $m$ )

$$\frac{E}{m} = \frac{1}{2} (\dot{r}^2 + r^2 \dot{\phi}^2) - \frac{GM}{r} \quad (\text{C2})$$

$$= \frac{1}{2} V_{\text{per}}^2 - \frac{GM}{R_{\text{per}}} = \frac{1}{2} V_{\text{apo}}^2 - \frac{GM}{R_{\text{apo}}} \quad (\text{C3})$$

yields the following expression for the perigee velocity in terms of perigee and apogee distances

$$V_{\text{per}}^2 = \frac{2GM R_{\text{apo}}}{R_{\text{per}}(R_{\text{apo}} + R_{\text{per}})} = \frac{2g_{\text{per}} R_{\text{per}} R_{\text{apo}}}{(R_{\text{apo}} + R_{\text{per}})} \quad (\text{C4})$$

510 where  $g_{\text{per}} = \frac{GM}{R_{\text{per}}^2}$  is the value of Earth's gravitational acceleration at geocentric distance  $R_{\text{per}}$ . The radial velocity  $\dot{r}$  satisfies

$$\dot{r}^2 = \frac{2E}{m} + \frac{2GM}{r} - \frac{(r^2 \dot{\phi})^2}{r^2} \quad (\text{C5})$$

$$= \frac{2E}{m} + \frac{2GM}{r} - \frac{R_{\text{per}}^2 V_{\text{per}}^2}{r^2}. \quad (\text{C6})$$

Differentiating this expression and dividing by  $2\dot{r}$  yields

$$\ddot{r} = -\frac{GM}{r^2} + \frac{R_{\text{per}}^2 V_{\text{per}}^2}{r^3}. \quad (\text{C7})$$

515 Evaluation at perigee  $r = R_{\text{per}}$  gives

$$\ddot{r}|_{r=R_{\text{per}}} = -\frac{GM}{R_{\text{per}}^2} + \frac{R_{\text{per}}^2 V_{\text{per}}^2}{R_{\text{per}}^3} = -\frac{GM}{R_{\text{per}}^2} + \frac{V_{\text{per}}^2}{R_{\text{per}}}. \quad (\text{C8})$$

Inserting the expression for  $V_{\text{per}}^2$  yields

$$\ddot{r}|_{r=R_{\text{per}}} = \frac{GM}{R_{\text{per}}^2} \frac{R_{\text{apo}} - R_{\text{per}}}{R_{\text{apo}} + R_{\text{per}}} = g_{\text{per}} \varepsilon \quad (\text{C9})$$

where  $\varepsilon = \frac{R_{\text{apo}} - R_{\text{per}}}{R_{\text{apo}} + R_{\text{per}}}$  is the orbital eccentricity. The altitude  $z$  is related to radial distance  $r$  and the Earth's planetary radius

520  $R_E$  through  $z = r - R_E$ . At perigee,  $t = 0$  and  $z = z_{\text{per}}$ . The parameter  $a_{\text{per}} = \ddot{z}(t = 0)$  coincides with the radial acceleration at perigee  $\ddot{r}|_{r=R_{\text{per}}}$ . Hence, orbital altitudes around perigee are approximately given by the quadratic function

$$z(t) \simeq z_{\text{per}} + \frac{a_{\text{per}}}{2} t^2. \quad (\text{C10})$$



To the same approximation order, the angular momentum conservation condition  $r^2\dot{\phi} = R_{\text{per}}V_{\text{per}}$  can be integrated to yield approximate azimuths  $\phi = \phi(t)$ . In  $\dot{\phi} = R_{\text{per}}V_{\text{per}}/r^2$  insert  $r = r(t) = R_{\text{per}} + \frac{a_{\text{per}}}{2}t^2$ , then expand

$$525 \quad \left(R_{\text{per}} + \frac{a_{\text{per}}}{2}t^2\right)^{-2} \simeq R_{\text{per}}^{-2} \left(1 - \frac{a_{\text{per}}}{R_{\text{per}}}t^2\right) \quad (\text{C11})$$

and integrate  $d\phi = R_{\text{per}}V_{\text{per}}r^{-2}dt$  to obtain

$$\phi(t) \simeq \frac{V_{\text{per}}}{R_{\text{per}}} \int_0^t \left(1 - \frac{a_{\text{per}}}{R_{\text{per}}}\tilde{t}^2\right) d\tilde{t} \quad (\text{C12})$$

$$= \frac{V_{\text{per}}}{R_{\text{per}}} \cdot \left(t - \frac{a_{\text{per}}}{3R_{\text{per}}}t^3\right). \quad (\text{C13})$$

The corresponding horizontal distances at the Earth's surface are then given by  $x = x(t) = R_{\text{E}}\phi(t)$ . By using Eq. (C9), this  
 530 can be further processed to yield

$$x(t) \simeq \frac{R_{\text{E}}V_{\text{per}}t}{R_{\text{per}}} \cdot \left(1 - \frac{\varepsilon}{3} \frac{g_{\text{per}}t^2}{R_{\text{per}}}\right). \quad (\text{C14})$$

The leading term is ground distance for a circular orbit. The correction produced by the second term is proportional to eccentricity.

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 535 workgroup at the Democritus University of Thrace (TS, ST, TB, DB, PP). JV developed the DIPCont methodology and the underlying theory, wrote the Python code and the first draft of the manuscript, and coordinated the writing of the paper. OM initiated LTI profile extrapolation under Daedalus Phase-0 science study, followed on by the activity of the SIFACIT team, and contributed text to Sections 1, 4, 5, 6. AB, LP, NS, and OM tested the DIPCont code and provided feedback for its improvement. SB, AB, OM, and LP checked the theory and the model derivations. TS, ST, TB, DB, PP contributed to early work on altitude reconstruction using simulation as well as rocket data, and the  
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