

1 Analysis of Orientation Errors in Triaxial Fluxgate

2 Sensors and Research on Their Calibration Methods

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11 **Abstract.** Three-axis magnetic flux gate sensors are widely used in Chinese geomagnetic observatories,
12 but due to their directional errors, it is necessary to study error correction methods to improve
13 measurement accuracy. Firstly, the mechanism of directional errors produced by three-axis magnetic
14 flux gate sensors is analyzed, followed by the development of measurement tools for conducting
15 directional error measurement experiments on the high-precision three-axis magnetic flux gate sensors
16 of the Chinese FGM-01 series. Experimental results show that correcting the Z-axis and D-axis
17 directional errors is essential. The observation data after error correction, whether in terms of the
18 standard deviation of its all-day baseline values or the relative difference magnitude with the reference
19 instrument, significantly decrease, demonstrating the clear correction effect and proving the
20 effectiveness of this correction method.

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22 **Keywords:** Tri-axis Magnetic Flux Gate Sensor, Orientation Error, Calibration

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24 1 Introduction

25 Three-axis fluxgate sensors have the advantages of high resolution, low power consumption, and low
26 cost, and are widely used in measuring the geomagnetic field signal (Langel et al.1988; Tohyama et
27 al.1988a,1988b; Ejiri et al.1988;Crassidis [and](#) Lai 2005). Currently, nearly 200 sets of three-axis
28 fluxgate magnetometers, mainly GM4 type (Figure 1a), GM4-XL type, and FGM-01 type (Figure 1b),
29 are installed in the Chinese geomagnetic observatories. Most observatories install two or more sets of
30 such instruments for parallel observations, aiming to ensure the continuity and integrity of the
31 observation data and to facilitate timely detection and identification of potential issues in the data. The
32 ideal measurement value of a three-axis fluxgate sensor should be equal to the true value of the
33 measured geomagnetic field variation(Luo et al.2019;Wu 2008). However, due to limitations in
34 manufacturing and installation processes, errors such as non-orthogonality, zero offset, and temperature
35 drift exist in three-axis fluxgate sensors unavoidably(Včelák et al.2006; Foster & Elkaim 2008; Pang
36 2011). Studies have shown that these errors can lead to deviations of the sensor's measurement values
37 from the true values of the measured geomagnetic field, significantly affecting its measurement
38 accuracy. Therefore, it is of great significance to correct the errors of the sensor(Zhu et al.2005;Li
39 2008).

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41 Research on the error of three-axis magnetic fluxgate sensors in the past has typically only considered
42 the systematic error of the sensors(Liu et al.2022), with relatively little study on the directional errors
43 introduced during sensor installation.Wang Xiaomei et al. (2017) analyzed the variation patterns
44 between the orientation of the instrument, the level of the base, and the observed data of each
45 component of the geomagnetic field based on theoretical calculations and station experiments,

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46 providing quantitative relationships. Liu Cheng et al. (2019) established a three-axis calibration model
 47 for the magnetic fluxgate magnetometer, determined the attitude angles and scale factor coefficients of
 48 the instrument, and then corrected the actual observation data based on the calculation results. The
 49 author once developed a measuring device in 2016 to measure and correct the directional errors of the
 50 D magnetic axis, eliminating the daily variation distortion recorded by the magnetic fluxgate
 51 magnetometer at Hongshan Observatory. However, the aforementioned algorithms or measurements
 52 are somewhat difficult (Zhu 2004) and not easy to implement, or only focus on the method of
 53 correcting the directional errors of the sensor's D magnetic axis, without yet conducting research on
 54 correcting the directional errors of the Z magnetic axis, all of which have shortcomings that need
 55 improvement.

56 This study analyzes the mechanism of directional error generation of the three-axis magnetic flux gate
 57 sensor, measures the directional error of the sensor using homemade measurement tools, and corrects
 58 the measurement results when reorienting. Finally, by comparing the changes in the actual
 59 measurement data before and after correction, the correction effect is analyzed.
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62 (a) GM4 Type Fluxgate Magnetomete



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64 (b) FGM-01 Type Fluxgate Magnetometer

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67 Figure 1: Fluxgate Magnetometer
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71 2 Analysis of Directional Errors in Three-Axis Fluxgate Magnetometer Sensors

72 This article mainly analyzes the directional errors generated during the installation of a three-axis
 73 fluxgate magnetometer, ignoring the errors of the three-axis orthogonality. Therefore, during the
 74 experiment, it is assumed that the three-axis of the fluxgate sensor is in a perfectly orthogonal ideal
 75 state. When installing the fluxgate instrument, a sensor that measures the declination angle D is usually
 76 used for orientation. Currently, Chinese geomagnetic observatories typically orient sensors in the
 77 following manner (referred to as the traditional orientation method). The first step is to select a day
 78 with calm magnetic fields, adjust the base angle screws of the sensor to center two mutually
 79 perpendicular bubbles, thereby determining the orientation of the Z-magnetic axis. The second step is
 80 to rotate the sensor horizontally to control the output value of the magnetic declination angle D within
 81 the range of -50-50nT, thus determining the orientation of the D-magnetic axis. The orientation of the
 82 H-magnetic axis is determined as the D-magnetic axis is determined.

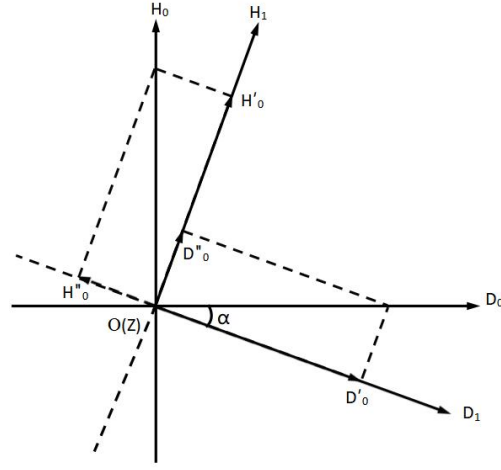
83 Assuming that the horizontal plane HOD of the three-axis fluxgate sensor is absolutely horizontal with
 84 the ideal coordinate system XOY, the angle of rotation of the sensor in the HOD plane with the H
 85 element as the axis is called the orientation error angle α (Wang et al., 2017). As shown in Figure 2,
 86 due to the presence of the orientation error angle α , the measurement values of the two elements in the
 87 horizontal plane mutually include each other's components. That is, the measurement value of the D
 88 element is the sum of the projections of the real D element and the H element in its measurement
 89 direction, which is expressed as

$$D_j = D'_0 - H''_0 = D_0 \cos \alpha - H_0 \sin \alpha$$

90 Similarly, the measurement value of the H element is

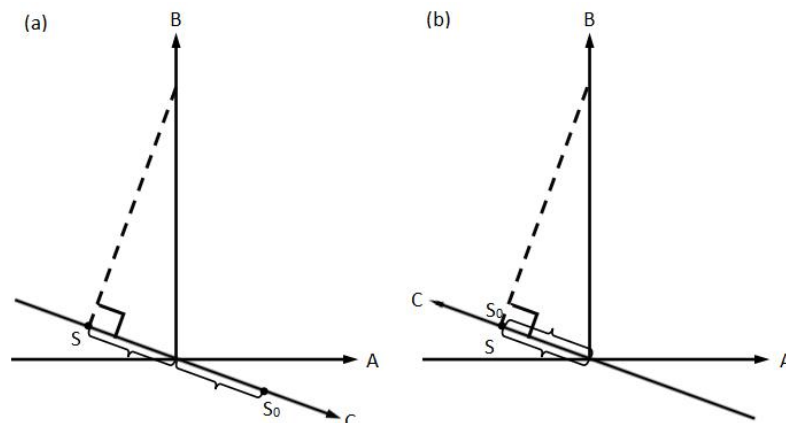
$$91 \quad H_1 = H'_0 + D''_0 = H_0 \cos \alpha + D_0 \sin \alpha$$

92 where D_0 and H_0 are the values of the magnetic field D and H elements in the ideal coordinate system,
93 D'_0 and D''_0 are the projections of the D element in the HOD plane when there is an orientation error
94 angle α , and H'_0 and H''_0 are the projections of the H element in the HOD plane when there is an
95 orientation error angle α . Since the value of the D element and α are relatively small, $D_0 \sin \alpha$ can be
96 omitted. Therefore, if there is an orientation error angle α , it has a greater impact on the recorded data
97 of the D element.



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100 **Figure 2 introduces the coordinate reference system of the magnetic sensor with the directional error**
101 **angle α .**

102 In traditional orientation methods, it is believed that controlling the output value of the magnetic
103 declination D within the range of -50 to 50 nT results in a relatively small orientation error angle.
104 However, due to some ferromagnetic substances inherent in the triaxial fluxgate sensor being
105 magnetized by the environmental magnetic field, residual magnetism is generated. This, combined with
106 zero drift produced by the sensor and data acquisition module, collectively superimposes a fixed
107 magnetic field on each axis of the fluxgate sensor, causing the measured magnetic field component
108 values to shift (Luo et al., 2019). Therefore, when the magnetic declination D is oriented, the output
109 value simultaneously includes the offset of the D magnetic axis, which may result in an increase in the
110 orientation error angle α , leading to inaccurate orientation of the D magnetic axis.
111 Assume the offset of the D magnetic axis is S_0 , and the projection value of the magnetic field H on the
112 D magnetic axis is S, as shown in Figure 3(a), where A represents the magnetic east direction, B
113 represents the magnetic north direction, and C represents the position of the magnetic axis when the
114 offset S_0 exists and the output value of D is zero. At this point, the output value of the D component is
115 $S_0 - S$; as shown in Figure 3(b), rotate the position of the D magnetic axis horizontally by 180° , and
116 the output value of the D element is $S_0 + S$; the numerical value of the offset S_0 can be obtained through
117 calculation.



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119 **Figure 3: Calculation schematic diagram of offset S_0 at the D magnetic axis orientation position (a) and its**
120 **position after rotating 180° (b).**

删除[Administrator]: 2 Analysis of Directional Errors in Three-Axis Fluxgate Magnetometer Sensors

Three-axis fluxgate magnetometer sensors consist of three identical and mutually orthogonal single-axis magnetic sensors.

When installing the orientation, the induction coil axis of the sensor should be aligned with the direction of the measured magnetic field. Currently, Chinese geomagnetic observatories typically orient sensors in the following manner (referred to as the traditional orientation method). The first step is to select a day with calm magnetic fields, adjust the base angle screws of the sensor to center two mutually perpendicular bubbles, thereby determining the orientation of the Z-magnetic axis.

The second step is to rotate the sensor horizontally to control the output value of the magnetic declination angle D within the range of -50-50nT, thus determining the orientation of the D-magnetic axis. The orientation of the H-magnetic axis is determined as the D-magnetic axis is determined.

Due to objective reasons such as manufacturing process limitations, it is difficult to make the Z-component coil plane consistent with the outer shape plane of the sensor. Adjusting the bubbles at the bottom of the sensor to be centered cannot ensure the horizontalness of the Z-component coil, causing the Z-magnetic axis to not completely point vertically to the Earth's core. The error that may result from this is referred to in this paper as the Z-magnetic axis directional error.

Furthermore, due to residual magnetism in the magnetic core, even if the spatial magnetic field intensity where the sensor is located is 0, there will still be a small offset output, causing the output value of the D-magnetic axis orientation to actually contain an offset value. This error is referred to as the D-magnetic axis directional error.

Assume the offset of the D magnetic axis is S_0 , and the projection value of the magnetic field H on the D magnetic axis is S, as shown in Figure 3(a), where A represents the magnetic east direction, B represents the magnetic north direction, and C represents the position of the magnetic axis when the offset S_0 exists and the output value of D is zero. At this point, the output value of the D component is $S_0 - S$; as shown in Figure 3(b), rotate the position of the D magnetic axis horizontally by 180° , and the output value of the D element is $S_0 + S$; the numerical value of the offset S_0 can be obtained through calculation.

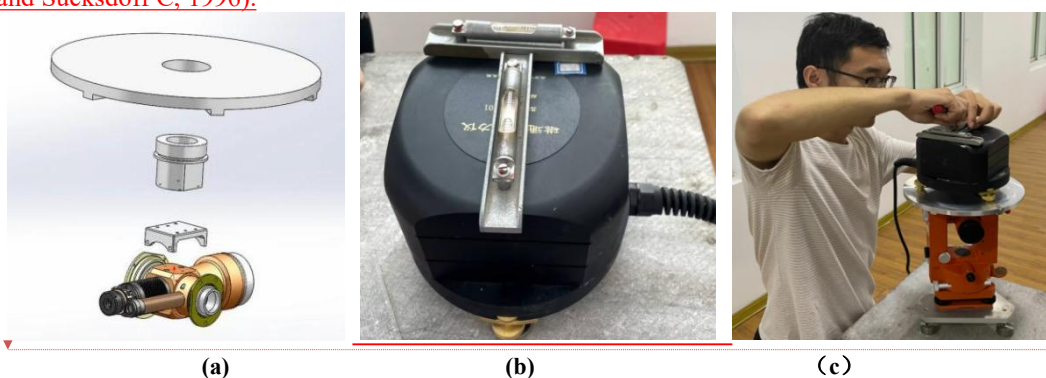
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121 Furthermore, the angle error caused by the non-horizontal placement of the triaxial fluxgate
 122 magnetometer will also lead to mutual influences among the components. Therefore, whether the
 123 leveling bubble of the instrument base can ensure that the Z magnetic axis is vertical is also crucial for
 124 accurate orientation.
 125 In summary, when installing and orienting the instrument, to ensure accurate orientation, in addition to
 126 considering the magnitude of the D output value during orientation, it is also necessary to consider the
 127 offset of the D magnetic axis, and at the same time, ensure whether the Z magnetic axis is truly in a
 128 vertical state.

129 **3 Experiment Introduction**

130 To complete this experiment, a set of non-magnetic rotary platform (hereinafter referred to as the
 131 platform) was specifically designed. This platform mainly consists of a weak magnetic plate and a non-
 132 magnetic theodolite. The weak magnetic aluminum plate is installed on the non-magnetic theodolite
 133 telescope (Figure 4a), and it enables the platform to rotate on a horizontal plane by adjusting the
 134 vertical dial and horizontal dial of the theodolite. During the experiment, first, adjust the level of the
 135 theodolite, then adjust the vertical dial to make the platform horizontal, then place the sensor on the
 136 platform, and check the verticality of the Z magnetic axis by rotating the horizontal dial and observing
 137 the output value of the Z magnetic axis. The offset of the D magnetic axis can be measured by
 138 adjusting the theodolite horizontal dial.

139 Before the experiment, two adjustable spirit levels with an accuracy of 10s, perpendicular to each other,
 140 were fixed on the top of the sensor with rosin, one of which passes through the magnetic axis (Figure
 141 4b). When the Z axis reaches the ideal vertical state, adjust the spirit level to a horizontal state so that
 142 when the sensor is installed in a new location, it can be placed in the same vertical position (Jankowski
 143 J and Sucksdoff C, 1996).



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 146 **Figure 4: Schematic assembly and actual operation of non-magnetic rotation platform**
 147 **(a) Non-magnetic rotation platform connection schematic diagram (b) Sensor top with external level (c)**
 148 **Actual operation of non-magnetic rotation platform**
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150 **3 Laboratory Determination and Calibration of Directional Deviation**

151 The measurement part of this experiment was conducted in the absolute measurement room of
 152 Hongshan observatory. The FGM-01 magnetic fluxgate magnetometer was used as the instrument
 153 under test (see Fig. 4c).

154 First, we examined the perpendicularity of the Z magnetic axis using the platform. After leveling the
 155 non-magnetic theodolite, we began adjusting the sensor's base angle screws to center two mutually
 156 perpendicular bubbles. By rotating the platform, we recorded the output values of the Z element at four
 157 positions 90° apart, as shown in Table 1. From the first set of data, it can be observed that the output
 158 values of the Z element at the four positions are not equal. The maximum difference between the two
 159 values at positions 180° apart reaches 749nT, indicating that the sensor's leveling with the bubbles does
 160 not accurately represent the perpendicularity of the Z magnetic axis, suggesting the presence of
 161 directional error. We continued adjusting the three base screws to make the Z element's output values
 162 as close as possible at different positions. Data from the 2nd to the 6th sets represent the stepwise
 163 adjustment of the Z component output values by the base screws. The data from the 6th set are the
 164 measurement results when the base screws are adjusted to their limits. At this time, the difference
 165 between the two values of the Z component at positions 180° and 90° apart is 1nT and 22nT,
 166 respectively. Since the measurement experiment was not conducted in a uniform magnetic field
 167 laboratory, even during a quiet magnetic period, there will still be small diurnal variations, making it

删除[Administrator]: Through the above analysis, this paper will measure the offset of sensor D magnetic axis using a homemade measuring tool, inspect the verticality of the Z magnetic axis, and correct the test results during reorientation. The measuring tool, a non-magnetic rotating platform (hereinafter referred to as the platform), is a customized weak magnetic aluminum plate. During measurement, the platform is first mounted on the theodolite telescope (Figure 4a), and then the sensor is placed on the platform. The sensor's rotation is achieved by adjusting the scale of the theodolite (Figure 4b). To check and correct the orientation error of sensor Z magnetic axis, two adjustable levelers are fixed at the top of the sensor in a mutually perpendicular manner using rosin before measurement (Figure 4c).



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168 difficult to achieve an ideal state where the Z component remains unchanged at any position when
 169 rotating the platform. There is a certain error. The maximum difference between the Z component
 170 values at different positions is 22nT. If this value is projected onto the magnetic declination D direction,
 171 compared to the output value range of -50-50nT when the magnetic declination D is oriented, its
 172 impact is small. Therefore, we believe that the Z magnetic axis is now in a vertical position. Obviously,
 173 the bubbles of the instrument itself are no longer centered, and we level a pair of external levels
 174 previously fixed on top of the sensor.

175 Subsequently, we measured the offset of the D magnetic axis according to the method shown in Figure
 176 2. By rotating the platform, we read the output values of the D element in two directions 180° apart,
 177 and calculated the D magnetic axis offset to be 109nT. Using the formula to convert the D magnetic
 178 axis offset from nT to angle, it is expressed as: $\theta = \arcsin \frac{S_D}{H}$. In the formula, H takes the annual average
 179 value of the H component. The known H value of Hongshan Station is 29,600 nT, and the θ value can
 180 be calculated to be approximately 0.2°.

181 Finally, the instrument under test was moved to the relative recording room of the Hongshan
 182 observatory. We first checked and leveled the external bubbles fixed at the top of the sensor to correct
 183 the Z magnetic axis directional error. Then, we adjusted the sensor to ensure the output value of the D
 184 element to be (109±50) nT, completing the correction of the D magnetic axis directional error, and
 185 initiating the instrument to begin recording observations.

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 187 **Table 1 Adjustment Results of the FGM-01 Instrument for the Verticality of the Z Magnetic Axis**
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Level Angle	Z-Element Output Value (nT)					
	1	2	3	4	5	6
290°	215	198	85	155	-150	-158
200°	-59	-131	-177	-115	-134	-135
110°	-534	-518	-403	-161	-160	-157
20°	-215	-146	-94	-127	-142	-136

189 It should be noted that we know the daily variation of the geomagnetic field is very small. When
 190 conducting experiments, it is advisable to choose a period when the magnetic field is calm and the
 191 temperature is stable. It can be considered that at this time, the geomagnetic field is stable and uniform.

192 **4 Analysis of Results**

193 To verify the correction effects mentioned above, the data from the instrument before and after
 194 calibration was compared in the following two ways.

195 **4.1 Comparative analysis of calibration results for daily variation records accuracy**

196 The purpose of the calibration for daily variation records accuracy is to examine the accuracy of the
 197 fluxgate magnetometer in recording diurnal variation data. The specific method is as follows: On a
 198 selected day, an absolute measurement is carried out every hour, and two sets of valid data are obtained
 199 for each measurement. The precision and stability are measured by calculating the change in the
 200 baseline value and the standard deviation (Gao et al. 1991; Zhang and Yang 2011). The tested
 201 instrument underwent diurnal variation calibration both before and after correction, with 10 absolute
 202 measurements each time, as shown in Figure 5. As can be seen from Figure 5, there is a clear diurnal
 203 variation pattern on the baseline value curves of the tested instrument before correction, with the
 204 maximum baseline value change D_B being 0.26', H_B being 1.7nT, and Z_B being 1.0nT, and the standard
 205 deviation for D_B being 0.07', H_B being 0.5nT, and Z_B being 0.3nT. After correction, the maximum
 206 baseline value changes for each element were D_B being 0.07', H_B being 1.0nT, and Z_B being 0.6nT,
 207 with standard deviations of D_B being 0.02', H_B being 0.3nT, and Z_B being 0.2nT. Compared to the pre-
 208 correction data, there was a reduction in both the maximum baseline value changes and standard
 209 deviations for each element, with the D element showing the most significant decrease in maximum
 210 baseline value change, by 0.19'. The results indicate that the observational data accuracy of the tested
 211 instrument post-correction is significantly superior to that of the pre-correction, and it more truly
 212 reflects the diurnal variation of the geomagnetic field.

删除[Administrator]: The 6th set of data reflects the measurement result when the base angle screws were adjusted to their extreme positions, with a difference of only 1nT between the two values at positions 180° apart, revealing that the bubbles on the sensor were no longer centered. Additionally, we adjusted a pair of external bubbles previously fixed at the top of the sensor for leveling.

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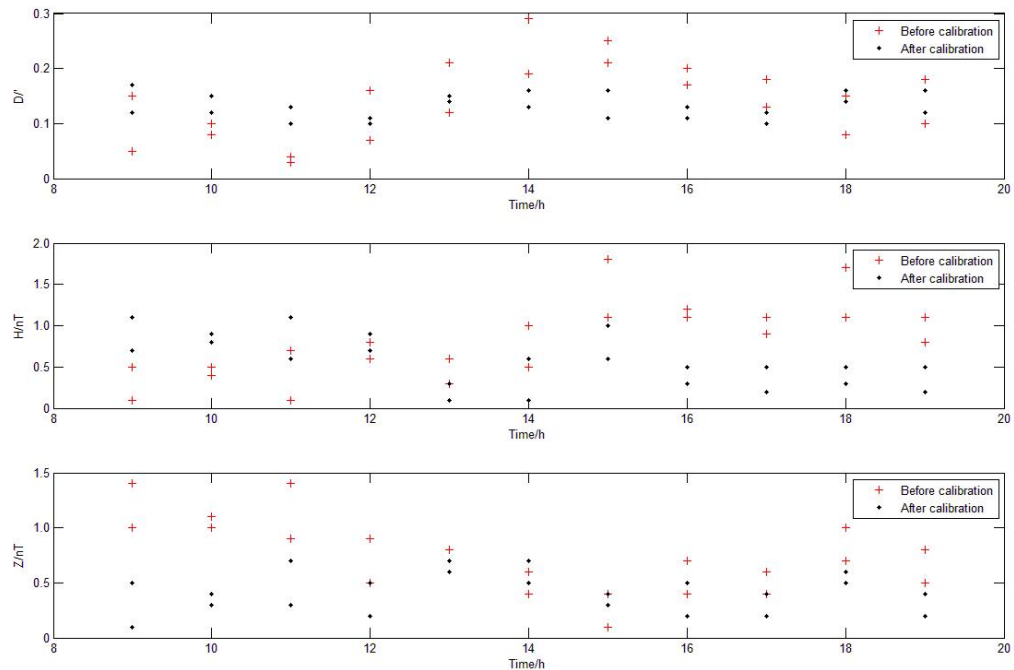


Figure 5: Baseline values obtained through daily calibration before and after calibration of the test instrument

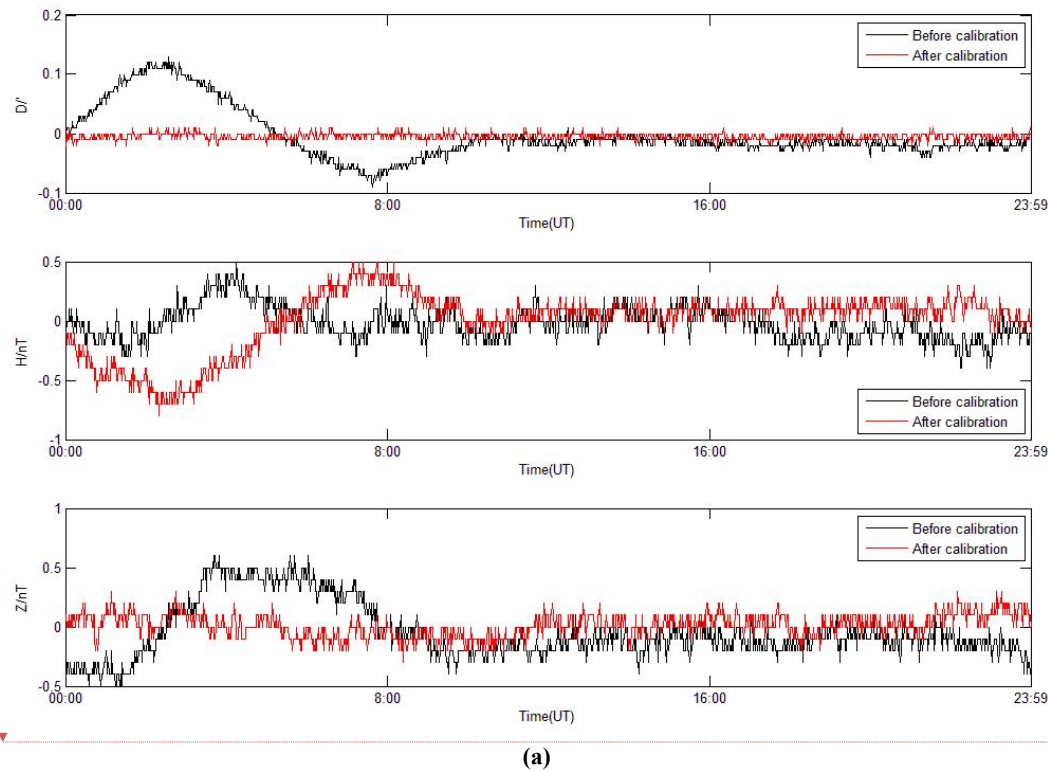
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217 4.2 The comparison of the difference curve of daily variation before and after instrument 218 calibration

219 The comparison of the difference curve of daily variation can generally describe the consistency of
220 data from different instruments at a station. Using the standard instrument GM4 located in the relative
221 recording room of Hongshan observatory as the reference instrument, the minute values of the
222 instrument under test are compared with those of the reference instrument. The difference curves
223 before and after correction are shown in Figure 6, where 6(a) and 6(b) respectively represent the
224 difference curves for geomagnetic quiet days and geomagnetic disturbed days. It can be observed that
225 the difference between the instrument under test and the reference instrument is significant before
226 calibration, especially for the D component. Even when the magnetic field is relatively stable, the
227 maximum variation in the difference of the D component still reaches 0.22'. After calibration, the
228 differences in magnetic field components between the instrument under test and the reference
229 instrument are significantly reduced, particularly for the D and Z components, with the difference
230 curves coming much closer to a straight line compared to the reference instrument.

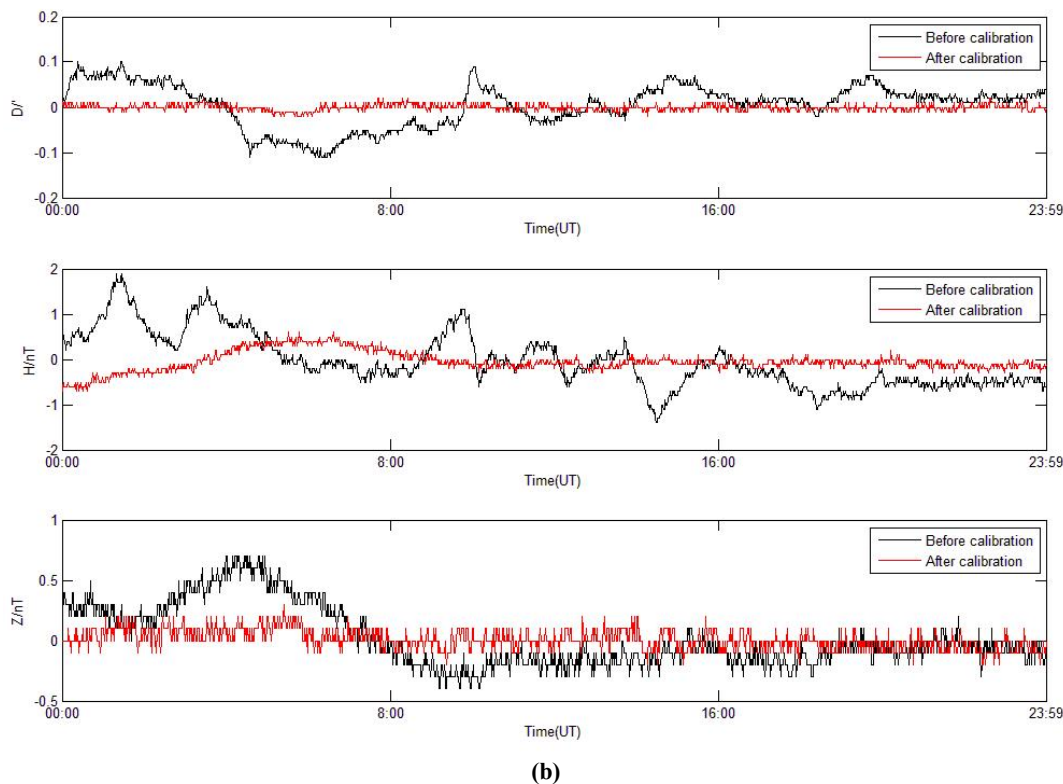
231 Select the observation data of the instrument before calibration (May 2022) and after calibration (May
232 2023) for comparison. From these data, respectively select five days of magnetically quiet days and
233 five days of magnetically disturbed days, and calculate the range of relative difference amplitude with
234 the reference instrument and its average range (Table 2). As can be seen from Table 2, the average
235 change range of the relative difference amplitude of the D and Z components before calibration is "
236 0.11 ~ 0.13' and -0.4 ~ 0.6nT", with the average change range of the amplitude being similar on
237 magnetically quiet days and magnetically disturbed days. The average change range of the amplitude
238 of the H component is almost twice as large on magnetically disturbed days compared to magnetically
239 quiet days. After calibration, the H component shows a slight decrease compared to before, and the
240 improvement effect of the D and Z components is very significant. The average change range of the
241 amplitude on magnetically quiet days is "-0.02 ~ 0.03' and -0.2 ~ 0.3nT", and on magnetically
242 disturbed days it is "-0.05 ~ 0.04' and -0.3 ~ 0.2nT", with the average change range of the amplitude
243 being significantly reduced compared to before calibration. This indicates that the above-mentioned
244 orientation method has a good calibration effect on the magnetic field components.

删除[Administrator]: The difference curves before and after correction are shown in Figure 6. geomagnetic quiet day and geomagnetic disturbance day are shown in Figure 6(a) and 6(b).



删除[Administrator]: Selecting data from five geomagnetically quiet days and five disturbed days before and after the calibration of the instrument under test, we computed the range of difference with the reference instrument and calculated the average amplitude (Table 2). As can be seen from Table 2, before calibration, the range of relative differences for the D and Z components were “-0.11 ~ 0.14’, -0.4 ~ 0.6nT” respectively, with the amplitude being roughly the same during quiet and disturbed days. For the H component, the amplitude of the difference was nearly double during disturbed days compared to quiet days. After calibration, the amplitude of the difference for the H component decreased slightly, while the improvement for the D and Z components was quite significant, with amplitudes during quiet days being “-0.02 ~ 0.03’ and -0.2 ~ 0.3nT” and during disturbed days being “-0.05 ~ 0.04’ and -0.3 ~ 0.2nT”, showing a marked decrease compared to before calibration. This indicates that the aforementioned calibration method is effective in correcting the magnetic field components.

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Figure 6: The difference curve between the tested instrument before and after calibration and the reference instrument
(a)geomagnetic quiet day (b)geomagnetic disturbance day

Table 2 The Range of Relative Difference Amplitudes Between the Test Instrument and the Reference Instrument

删除[Administrator]: The change amplitude of the daily variation difference between the tested instrument and the reference instrument on a daily basis

	before calibration			after calibration				
	Date	D (°)	H (nT)	Z (nT)	Date	D	H	Z
Magnetic Quiet Day	1 May	-0.11 ~ 0.12	-0.7 ~ 1.0	-0.4 ~ 0.6	5 May	-0.02 ~ 0.03	-0.7 ~ 0.6	-0.3 ~ 0.2
	19 May	-0.12 ~ 0.13	-0.4 ~ 0.8	-0.3 ~ 0.8	8 May	-0.02 ~ 0.02	-0.5 ~ 0.4	-0.2 ~ 0.2
	20 May	-0.11 ~ 0.16	-0.5 ~ 0.4	-0.4 ~ 0.4	19 May	-0.03 ~ 0.03	-0.5 ~ 0.4	-0.2 ~ 0.3
	21 May	-0.11 ~ 0.12	-0.5 ~ 0.3	-0.5 ~ 0.6	21 May	-0.01 ~ 0.03	-0.4 ~ 0.4	-0.3 ~ 0.3
	25 May	-0.09 ~ 0.14	-0.7 ~ 0.6	-0.4 ~ 0.7	25 May	-0.02 ~ 0.02	-0.6 ~ 0.6	-0.2 ~ 0.3
	Mean	-0.11 ~ 0.13	-0.6 ~ 0.6	-0.4 ~ 0.6	Mean	-0.02 ~ 0.03	-0.5 ~ 0.5	-0.2 ~ 0.3
Magnetic Disturbed Day	5 May	-0.11 ~ 0.13	-1.4 ~ 0.4	-0.3 ~ 0.9	1 May	-0.02 ~ 0.04	-0.8 ~ 0.9	-0.3 ~ 0.3
	6 May	-0.12 ~ 0.09	-1.5 ~ 1.6	-0.5 ~ 0.5	11 May	-0.07 ~ 0.03	-1.3 ~ 1.0	-0.3 ~ 0.2
	8 May	-0.11 ~ 0.13	-0.8 ~ 1.2	-0.4 ~ 0.7	14 May	-0.07 ~ 0.05	-0.9 ~ 1.4	-0.2 ~ 0.3
	17 May	-0.13 ~ 0.16	-1.7 ~ 1.2	-0.6 ~ 0.6	15 May	-0.05 ~ 0.02	-1.0 ~ 0.8	-0.2 ~ 0.3
	31 May	-0.11 ~ 0.17	-1.3 ~ 1.0	-0.4 ~ 0.5	27 May	-0.03 ~ 0.05	-1.0 ~ 0.9	-0.3 ~ 0.1
	Mean	-0.12 ~ 0.14	-1.3 ~ 1.1	-0.4 ~ 0.6	Mean	-0.05 ~ 0.04	-1.0 ~ 1.0	-0.3 ~ 0.2

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259 5 Discussion and Conclusion

260 This paper has analyzed the generation mechanism of orientation errors in triaxial fluxgate
 261 magnetometers and conducted a station experiment on an FGM-01 instrument using a self-made
 262 measurement device. The experimental and research results show that orientation errors occur in both
 263 the Z and D magnetic axes of the sensor, and it is necessary to correct these errors. The observational
 264 data, after correction for orientation errors, demonstrated a significant reduction in both the standard
 265 deviation of baseline values and the amplitude of differences when compared to a reference instrument,
 266 proving the effectiveness of the correction method. The measurement device used in the experiment is
 267 low-cost, simple to operate, and easy to disseminate, boasting a high performance-to-price ratio. In this
 268 study, the author found that the improvement effects on the D and Z components are more pronounced,
 269 whether on magnetically quiet or disturbed days, but not as significant for the H component. This
 270 indicates that the accuracy of geomagnetic daily variation records is influenced by factors other than
 271 orientation errors, including orthogonality, among others. We will continue to examine the impact of
 272 instrument orthogonality and correction methods in future work. The research presented in this paper
 273 provides a reference for the standardized installation and regular adjustment of orientation in fluxgate
 274 magnetometers at geomagnetic stations.

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276 Acknowledgments

277 The geomagnetic observation data in this article are sourced from the National Geomagnetic Network
 278 Center of the Institute of Geophysics, China Earthquake Administration. Senior Engineer Li Xijing
 279 from the Qianling Station in Shanxi Province proposed the measurement method for directional errors
 280 and guided the specific experimental procedures. We would like to express our gratitude here as well.

281 Funding Information

282 Supported by Science for Earthquake Resilience of China (XH23006A) and Special Project of
 283 Hongshan Scientific Observation of China (DZ2021110500003).

284 Competing Interests

285 The authors have no competing interests to declare.

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← --- 设置格式[Administrator]: 左

删除[Administrator]: Liu,C,et al.:Consistency correction for the observed data of fuxgate magnetometer based on geneticalgorithms,Progress in Geophysics,34(2):0751-0756,https://doi:10.6038/pg2019CC0024,2019.

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